

Challenges in Advanced Motion Control

Maarten Steinbuch

Control Systems Technology Group

DCSC symposium june 2004

/department of mechanical engineering

TU/e

TU Eindhoven



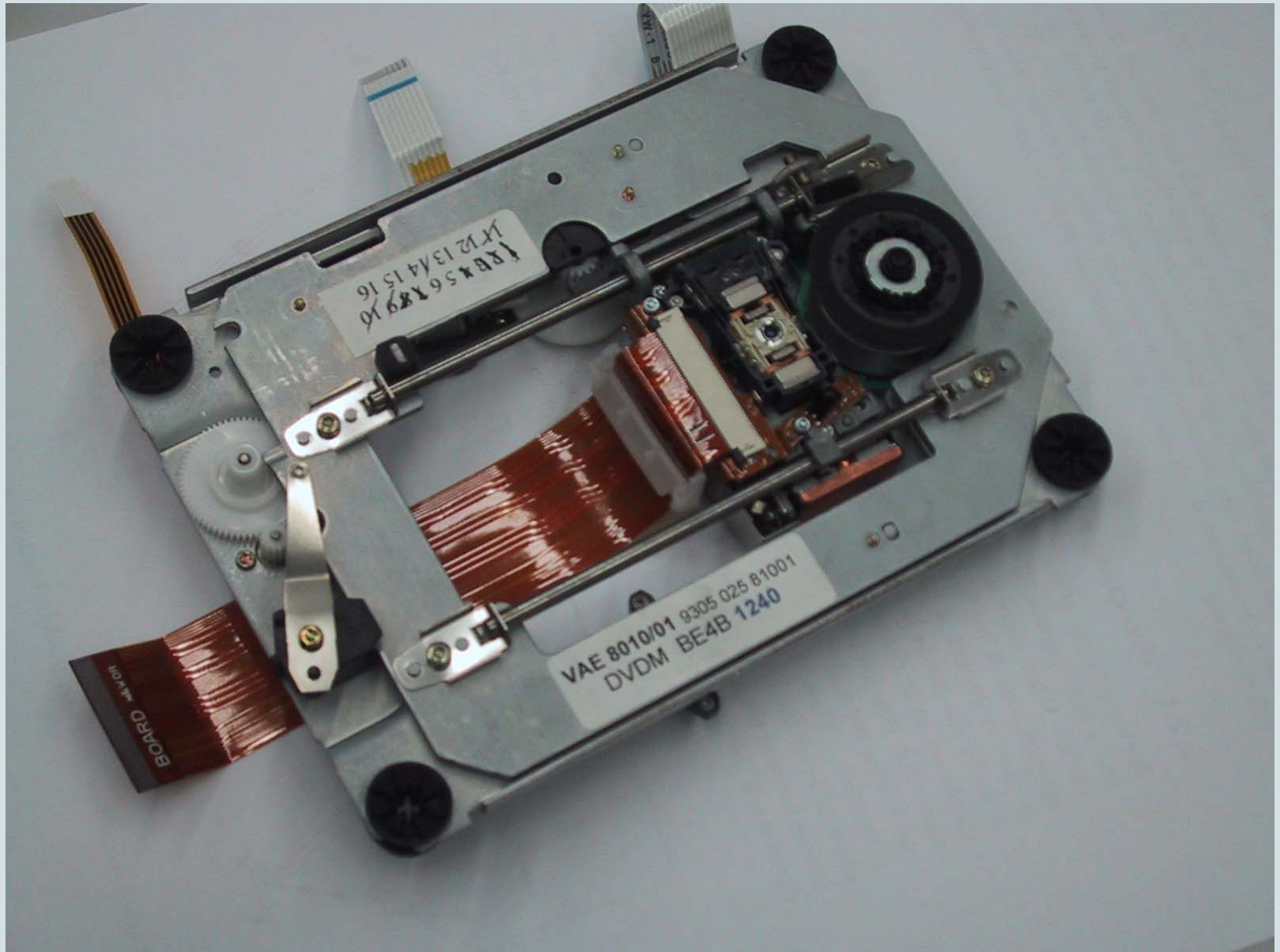
TU Delft



Philips

/department of mechanical engineering

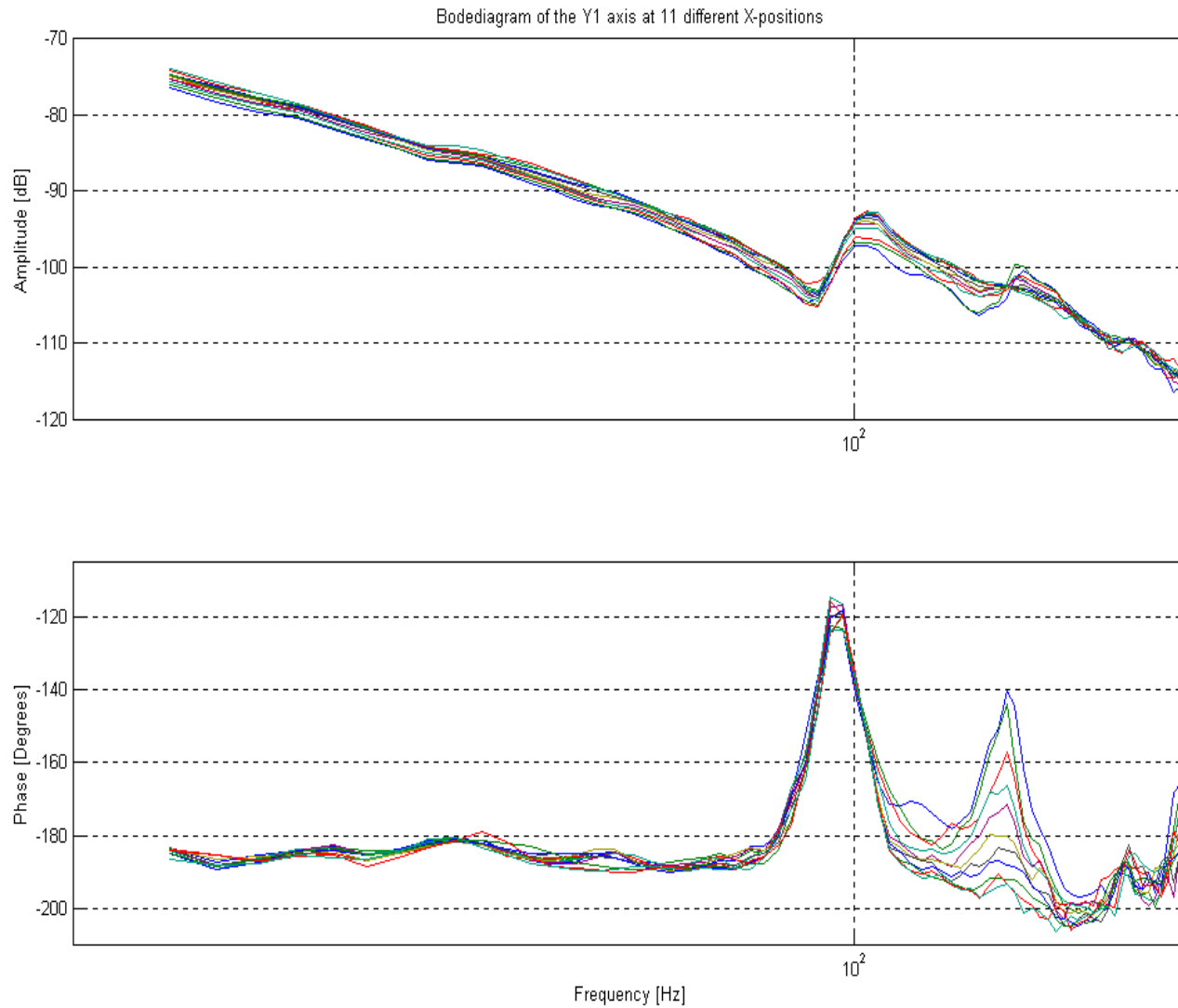
TU/e



TU/e

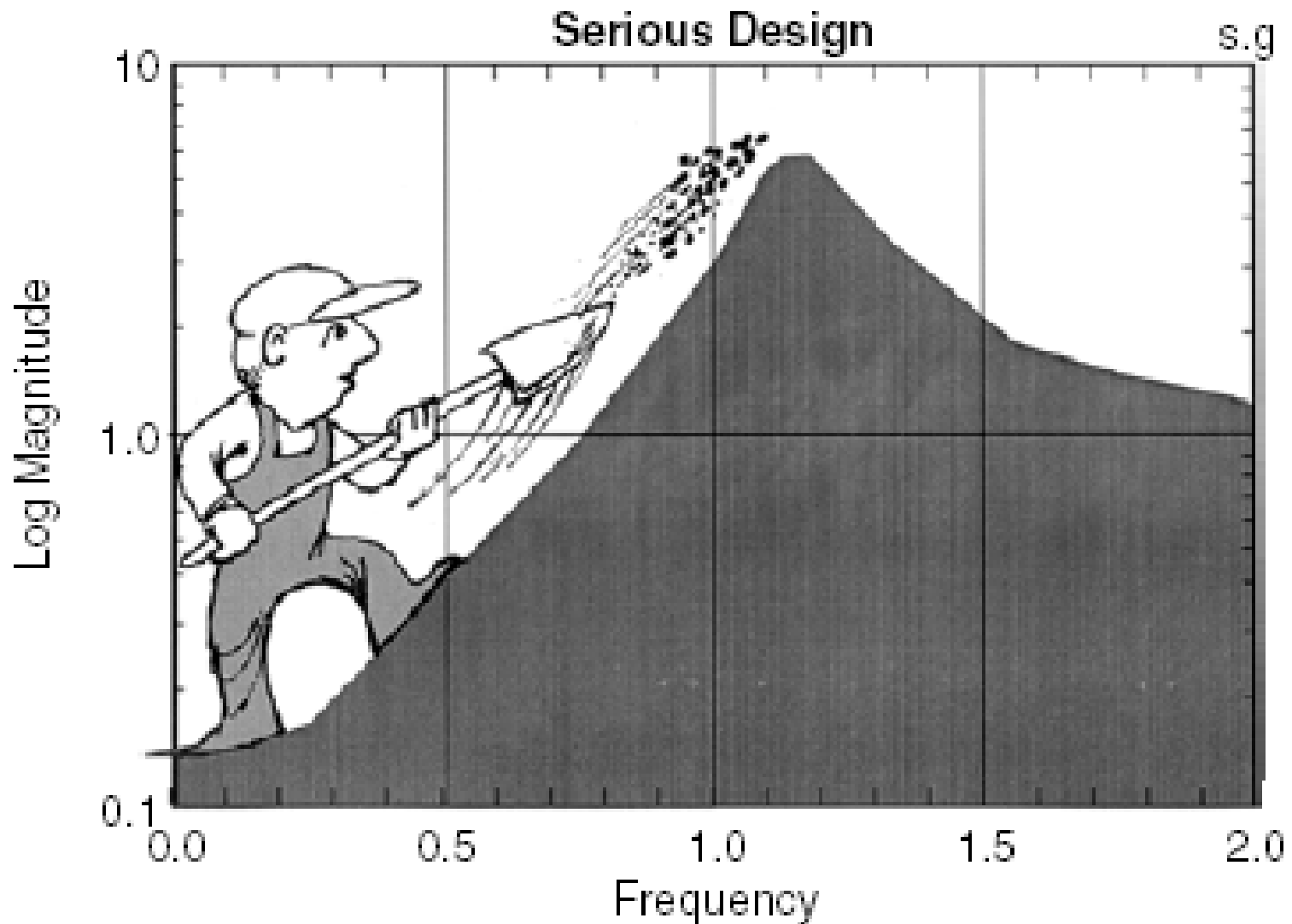


TU/e

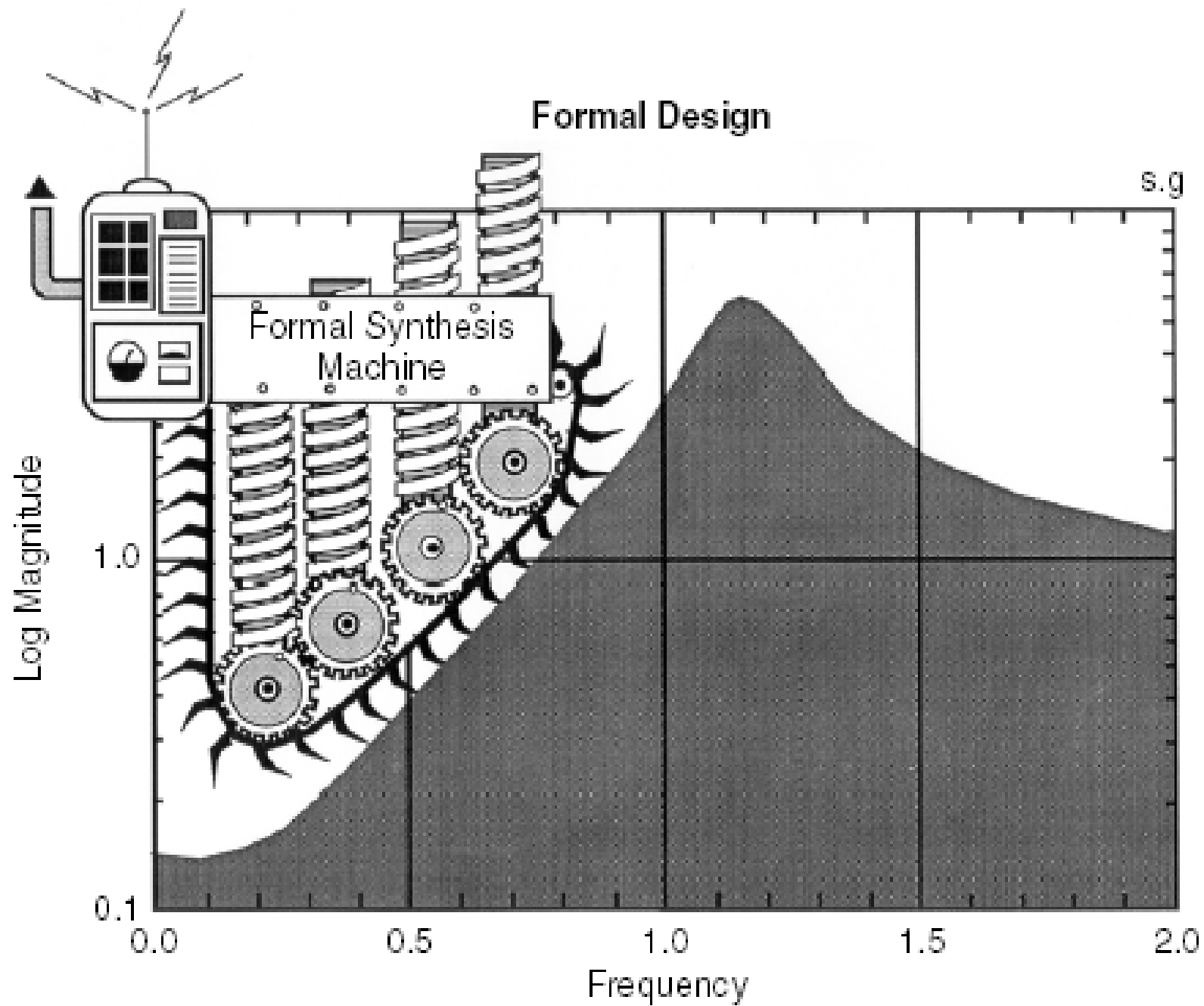


Motion Control Properties

- experimentation is ‘cheap’ (design cycle 7 min: FRF measurement, model, loopshape, implementation)
- plant decoupling, i.e. SISO
- feedforward: low-order model-based
- feedback: loopshaping
- key limitation: bode sensitivity integral
- finished?



Formal Design



Motion Control Challenge:

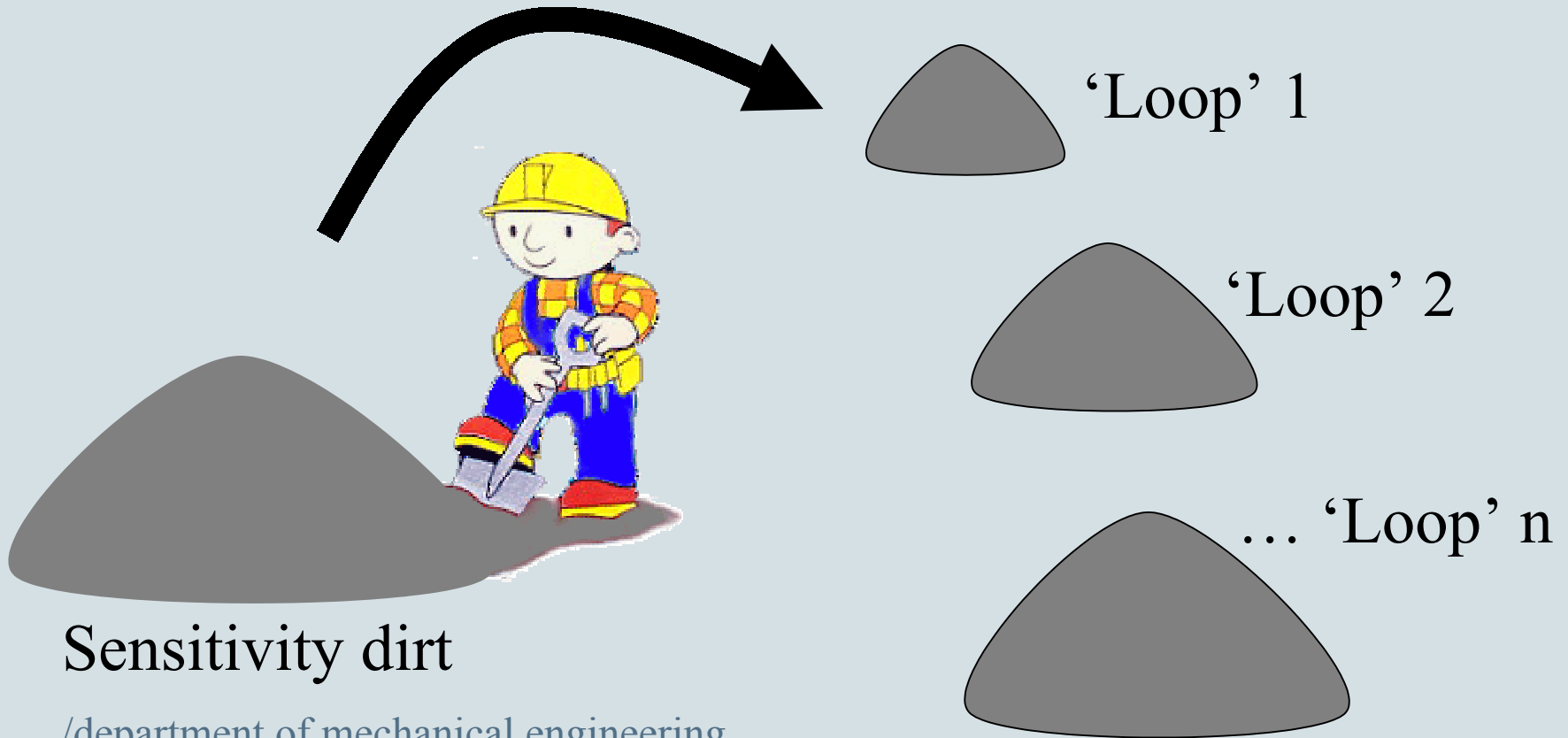
how to cope with Bode sensitivity limitation?

directions of motion control research

- nonlinear control of linear systems (reset...)
- MIMO loopshaping
- disturbance-based modelling and control
- data-driven control

TU/e

MIMO integral constraints...

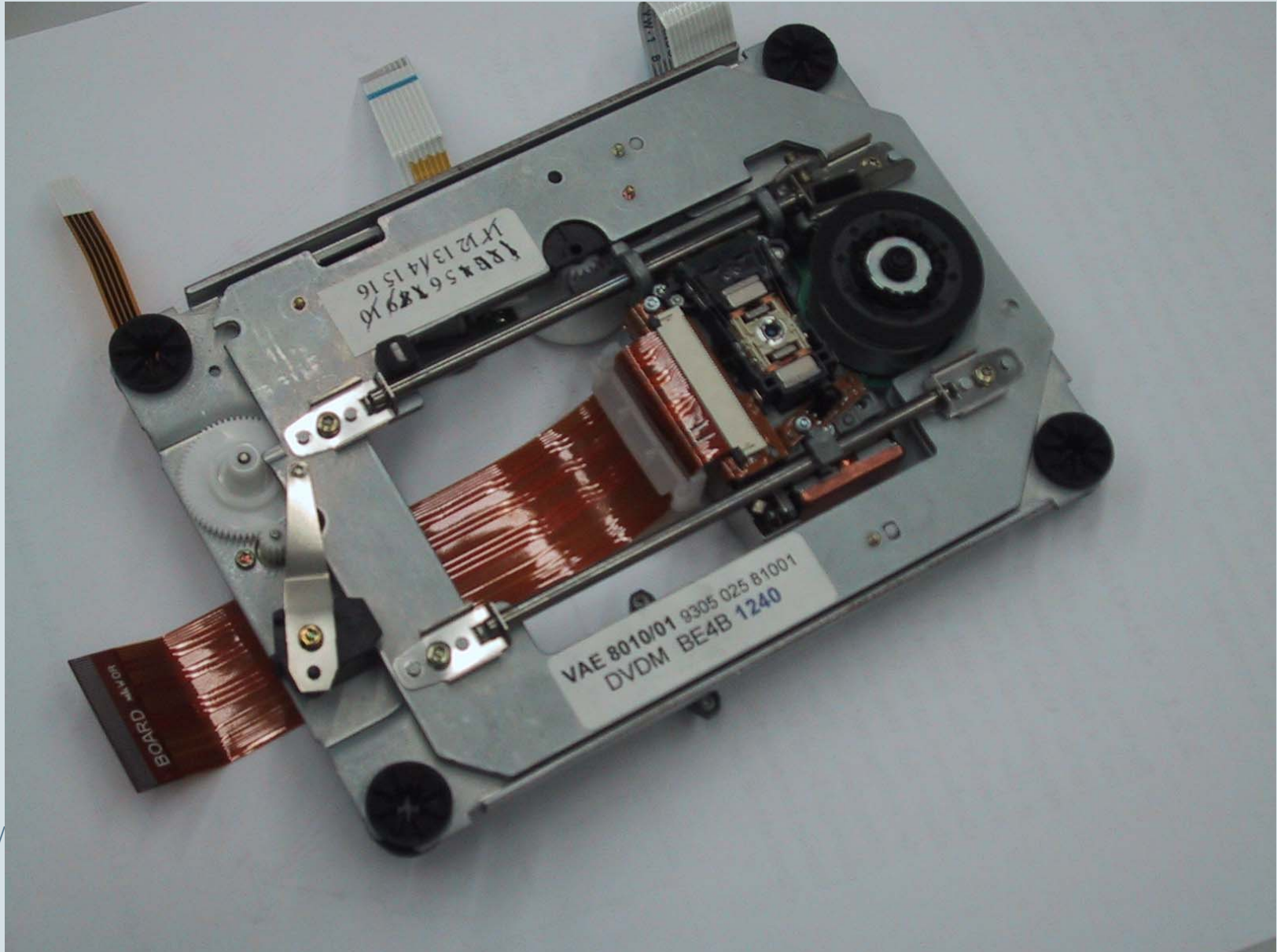


/department of mechanical engineering

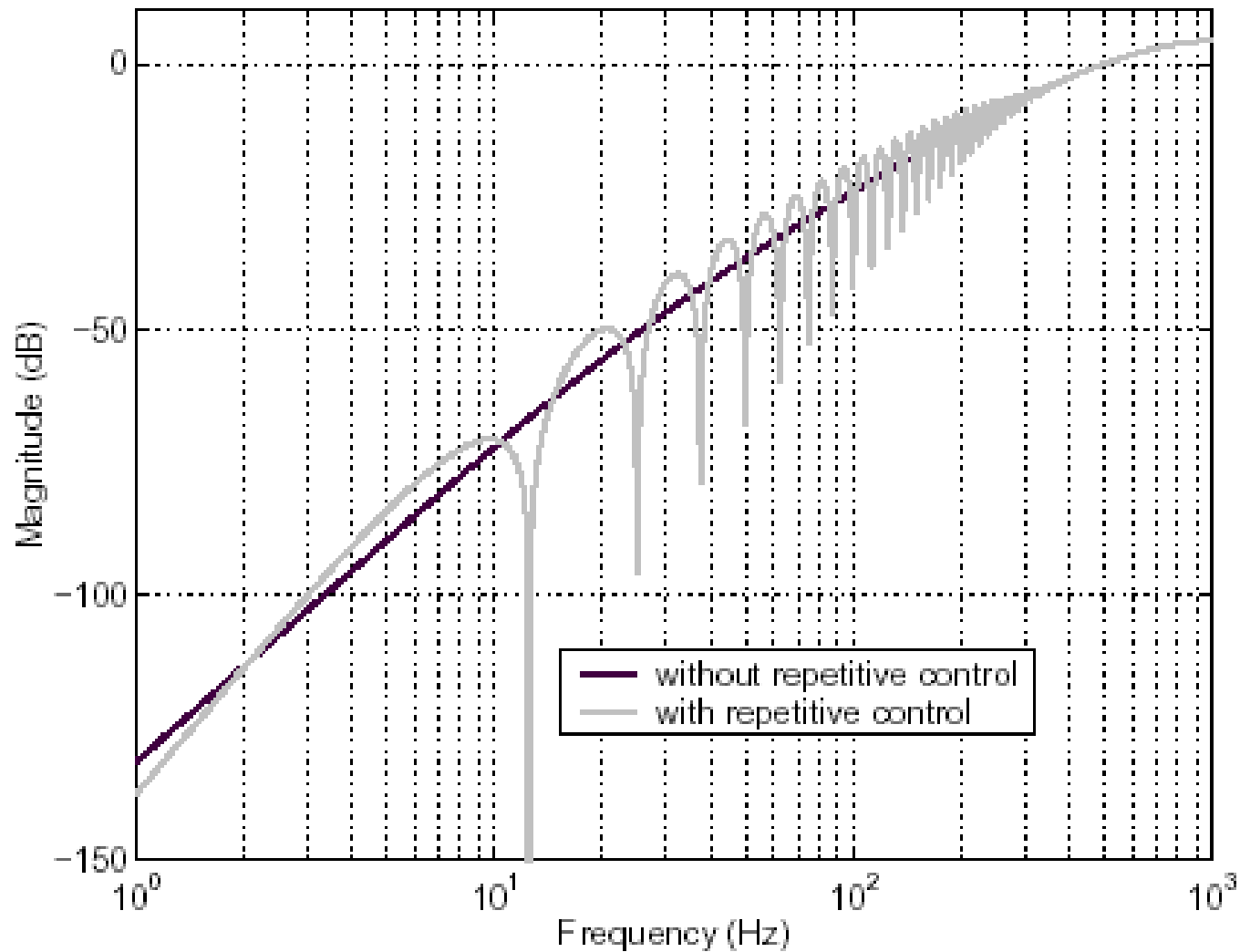
disturbance-based modelling and control

- disc errors vs shocks optical storage
- stochastic vs deterministic disturbances
- repetitive vs a-periodic setpoints or disturbances

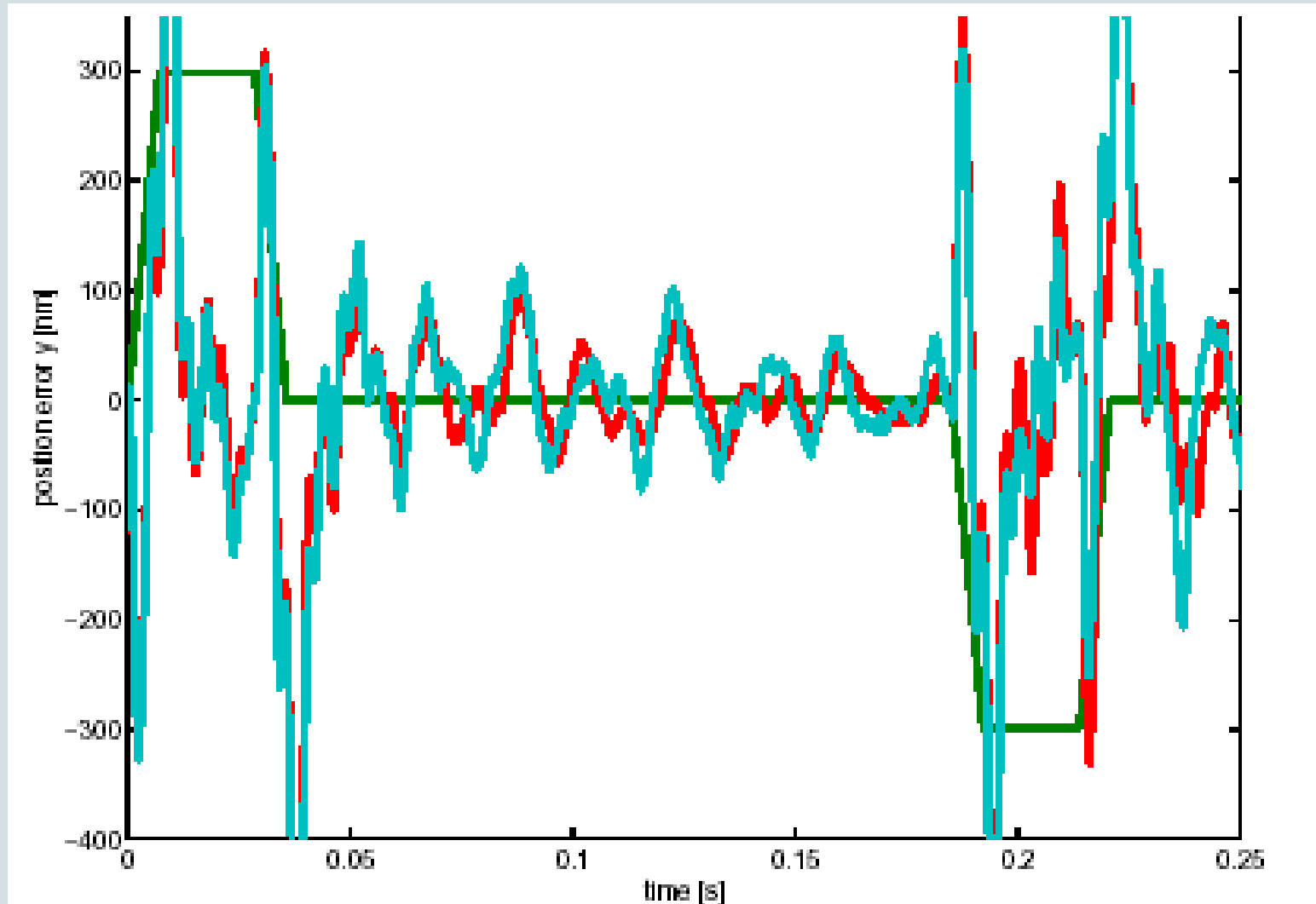
Internal model principle....



TU/e

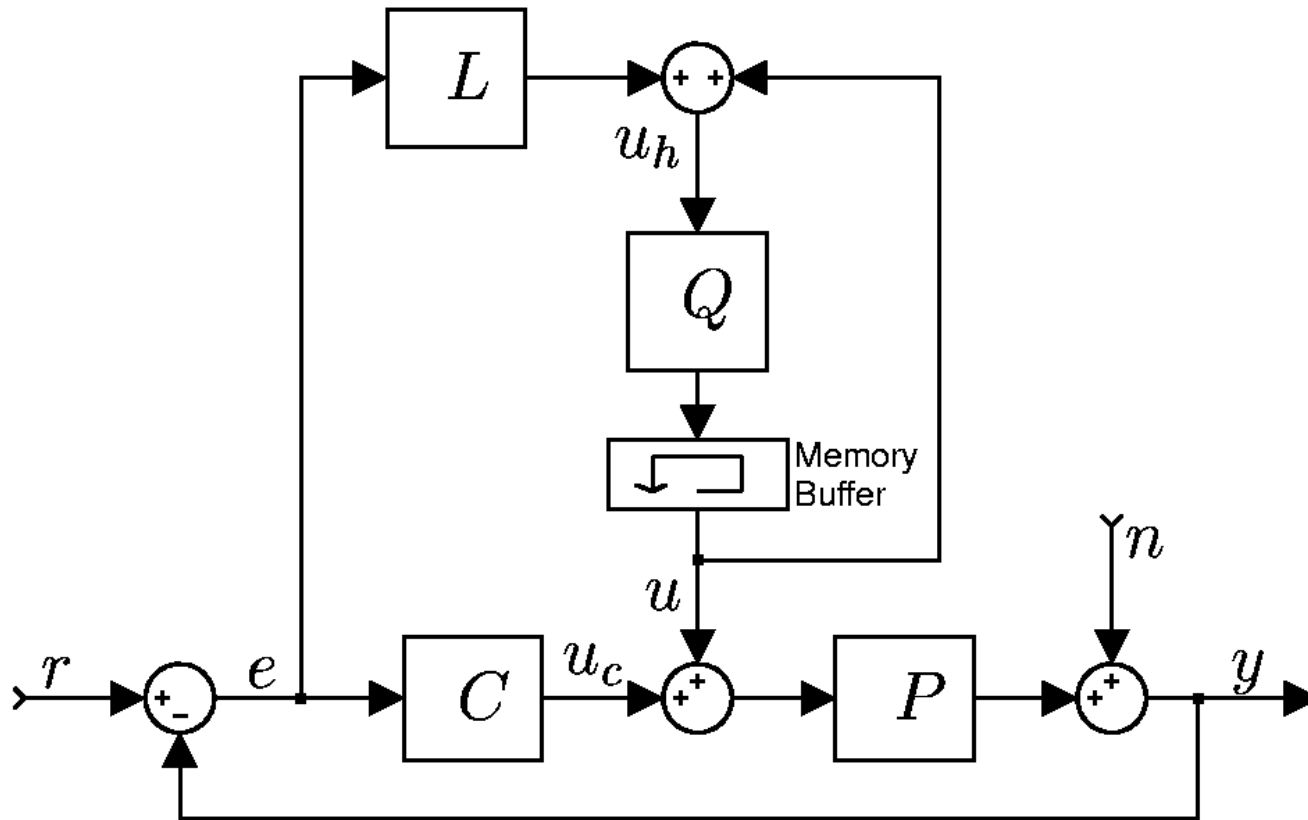


TU/e



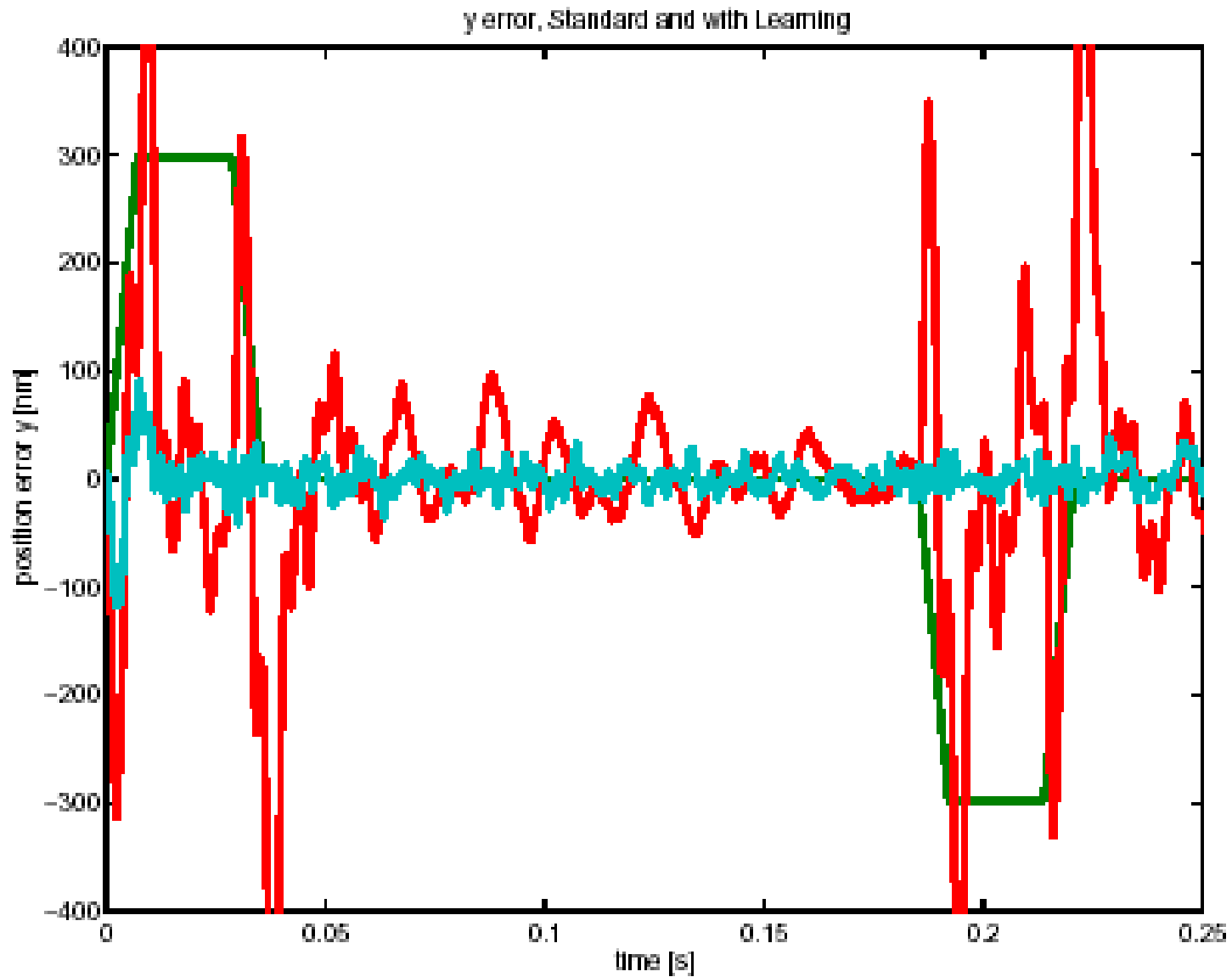
/department of mechanical engineering

Iterative Learning Control (ILC)



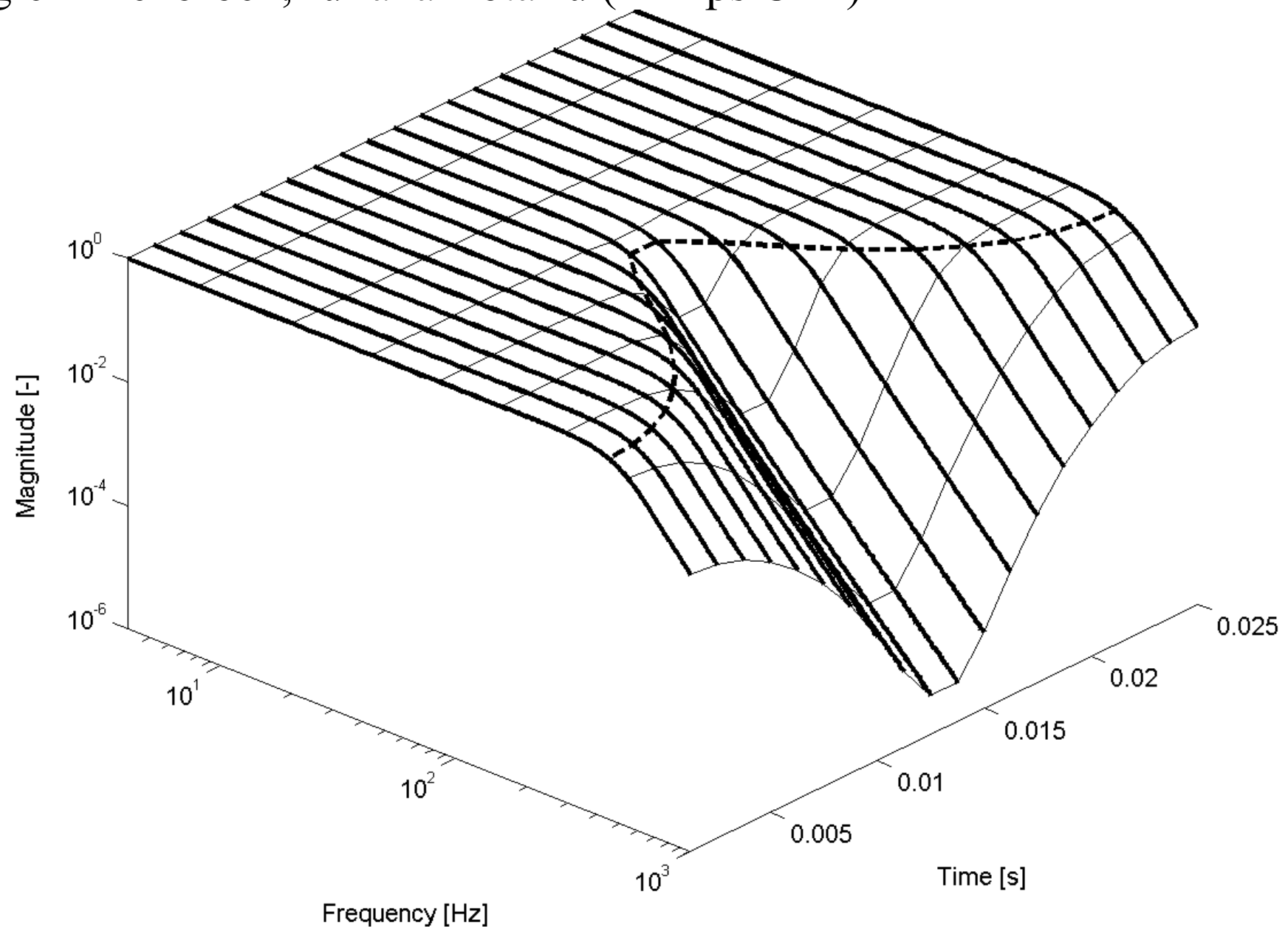
$$e_{k+1} < e_k \quad \leftarrow \quad |Q(1 - LPS)| < 1$$

TU/e

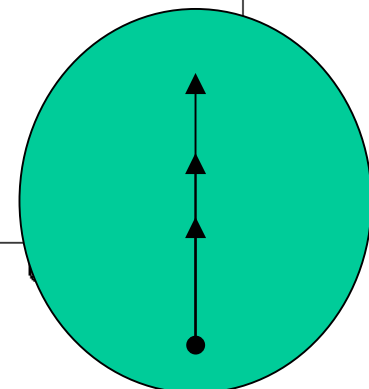
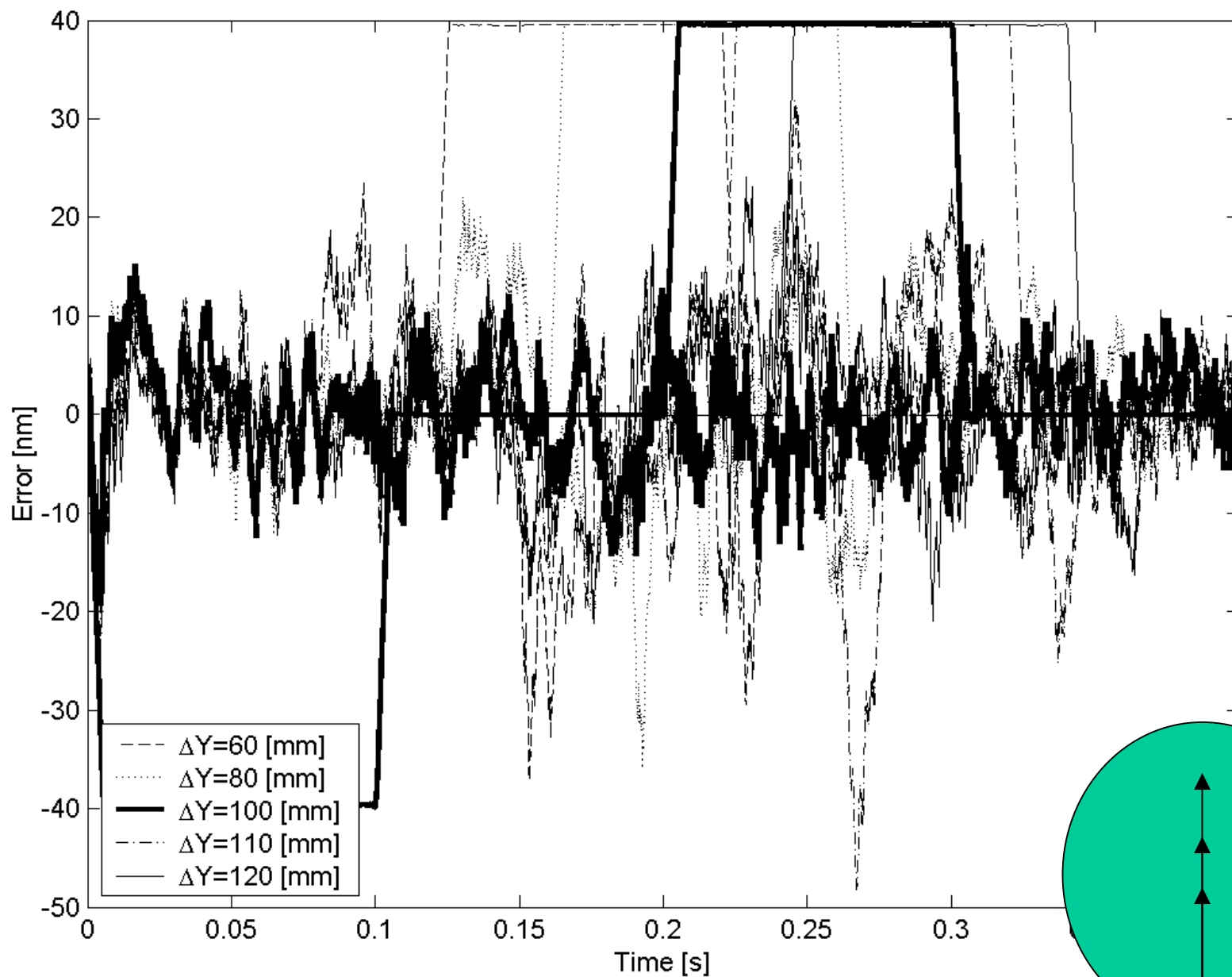


Time-frequency adaptive Iterative Learning Control

Rogier Ellenbroek, Iuliana Rotariu (Philips CFT)



Experimental results



directions of motion control research

- nonlinear control of linear systems (reset...)
- MIMO loopshaping
- disturbance-based modelling and control
- data-driven control

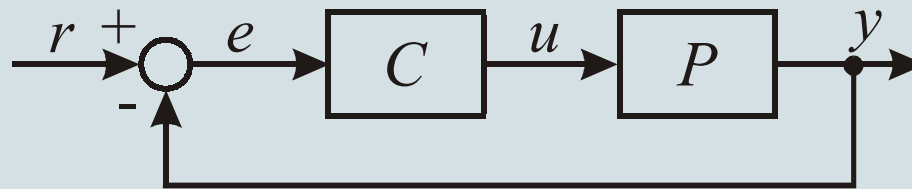
Data-based Design of High-performance Motion Controllers

Dragan Kostić

- Examples:
 - *data-based LQG control*
 - *unfalsified control*
 - *iterative feedback tuning*
 - *virtual reference feedback tuning*

Problem statement

- Design a SISO LTI controller C for LTI plant P



- Control objective: realize the desired S_o and T_o
- Ideal controller C_o :

$$S_o = \frac{1}{1+PC_o}, \quad T_o = \frac{PC_o}{1+PC_o}.$$

Data-based controller design

- The controller class: $\{C(z, \boldsymbol{\theta})\} = \{C_p(z) \boldsymbol{\beta}^T(z) \boldsymbol{\theta}\}$.
- $C_p(z)$ is directly prescribed by the designer: notches, integrators, etc.
- Basis functions: $\boldsymbol{\beta}(z) = [\beta_0(z) \beta_1(z) \dots \beta_n(z)]^T$.
- Tuning parameters: $\boldsymbol{\theta} = [\theta_0 \theta_1 \dots \theta_n]^T$.

TU/e **Data-based controller design**

- Constraint on C_o : $T_o(z) = C_o(z)S_o(z)P(z)$

- Model-based cost function:

$$J_{\text{MB}}(\boldsymbol{\theta}) = \|(T_o(z) - C(z, \boldsymbol{\theta})S_o(z)P(z))W(z)\|_2^2$$

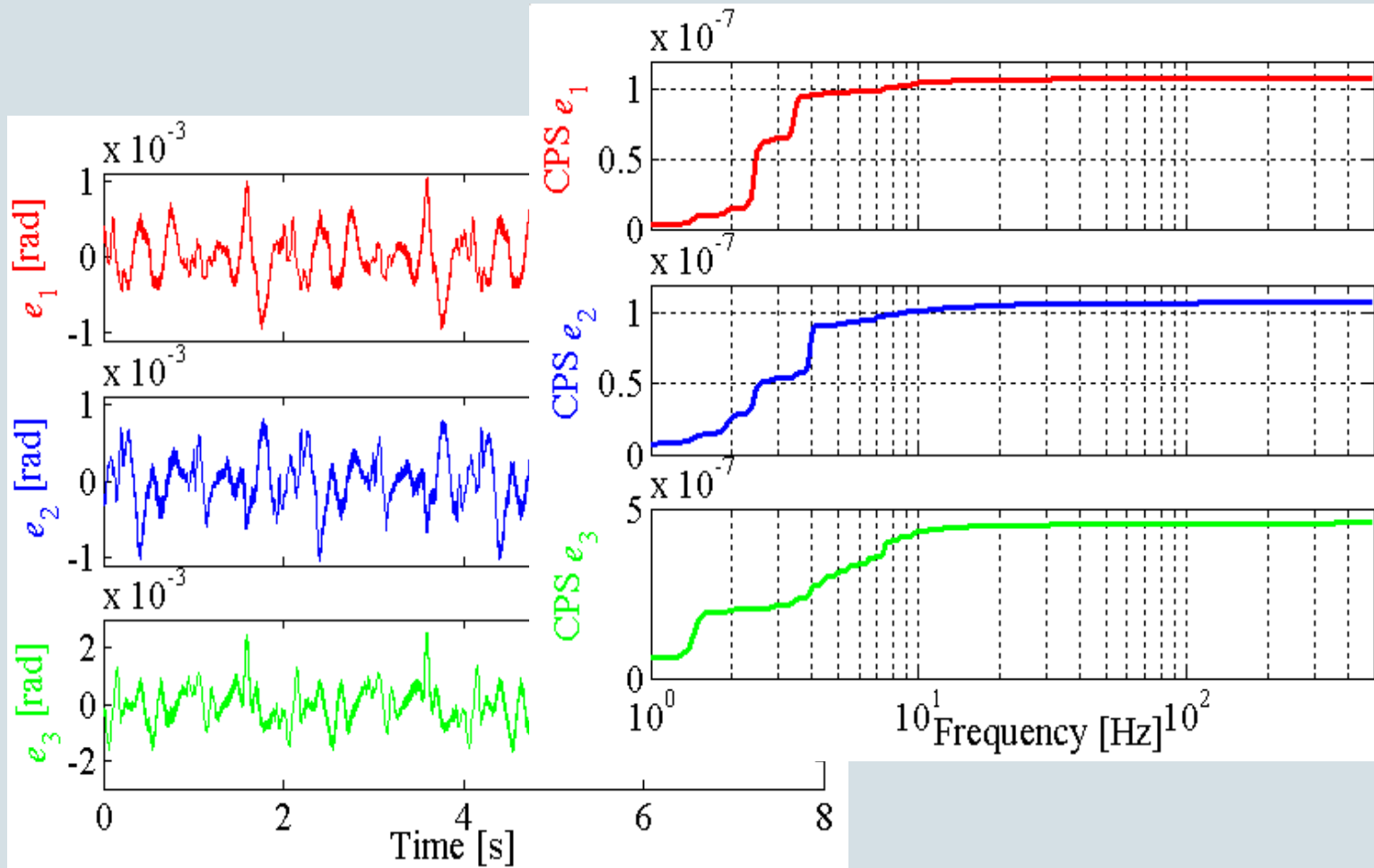
- Processing the measurements:

$$T_o(z)u(t) = C(z, \boldsymbol{\theta})S_o(z)P(z)u(t) \Rightarrow T_o(z)u(t) = C(z, \boldsymbol{\theta})S_o(z)y(t)$$

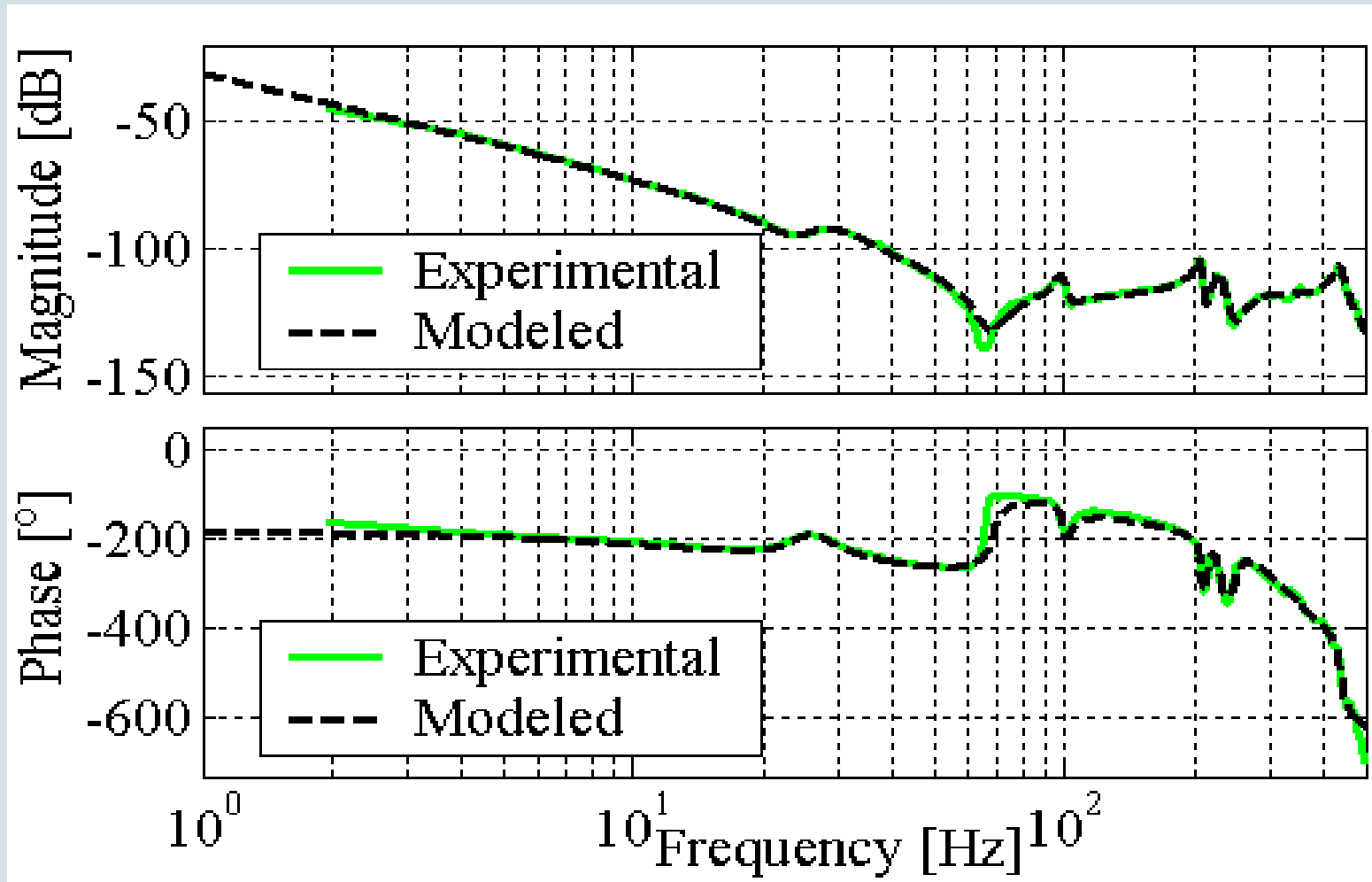
- Data-based cost function:

$$J_{\text{DB}}^N(\boldsymbol{\theta}) = \frac{1}{N} \sum_{t=1}^N [L(z)(T_o(z)u(t) - C(z, \boldsymbol{\theta})S_o(z)y(t))]^2$$

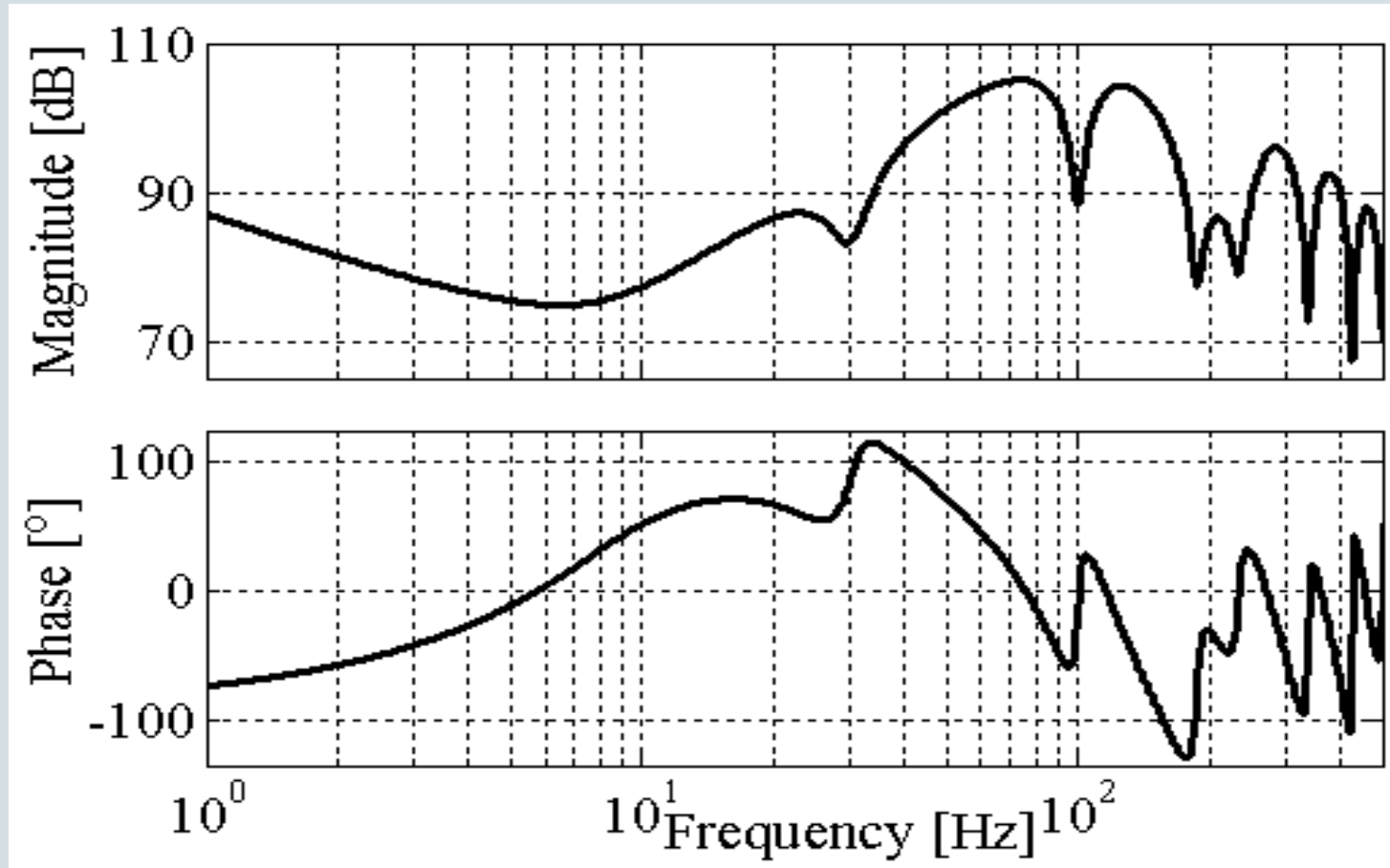
TU/e



TU/e



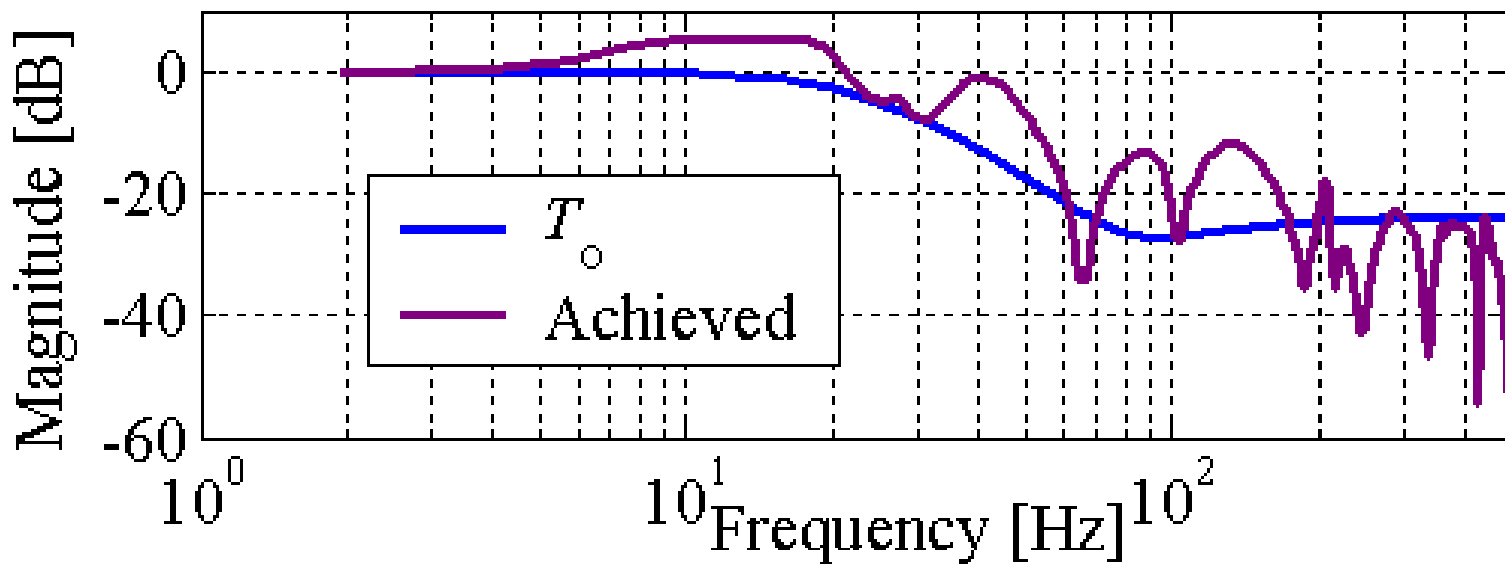
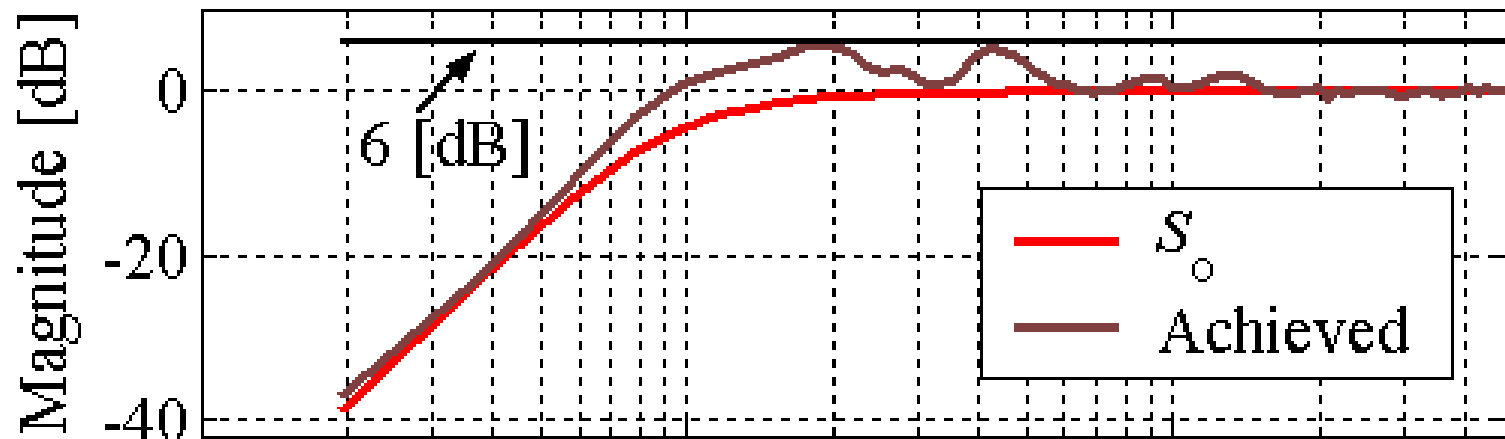
TU/e



/department of mechanical engineering

$$C_1(z, \hat{\theta}_{DB}^N)$$

TU/e

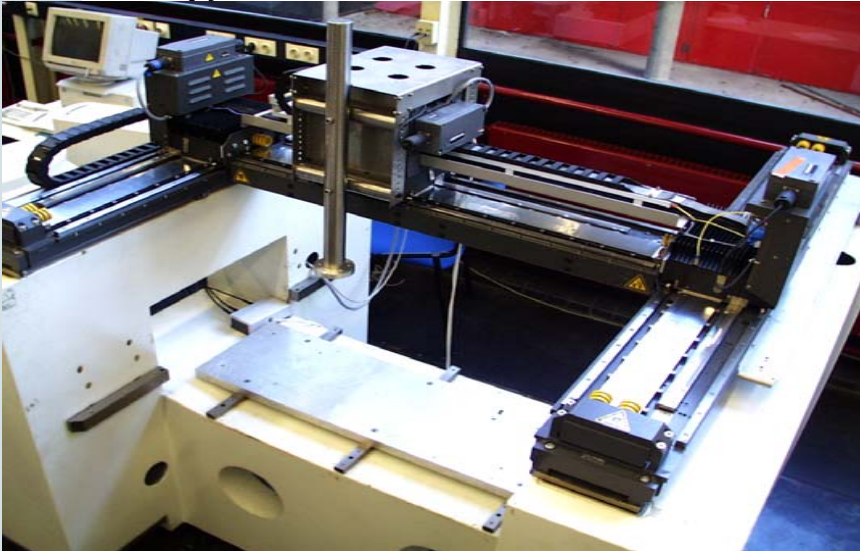
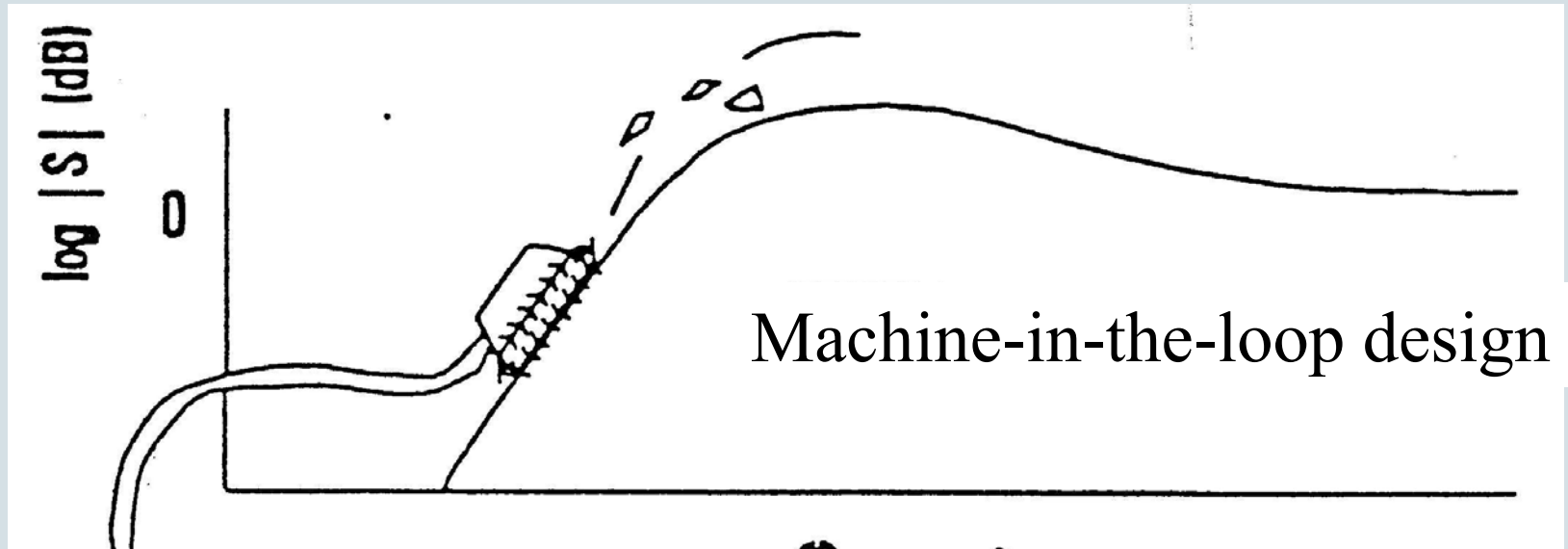


Motion Control Challenge:

how to cope with Bode sensitivity limitation?

directions of motion control research

- nonlinear control of linear systems (reset...)
- MIMO loopshaping
- disturbance-based modelling and control
- data-driven control



8 →

DCSC: Success!!!!!!