

Identificatie & Regelaar Tuning: Een Stukje Hardheid op de Tafel

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On the occasion of Prof. Bosgra 65th birthday



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Translate text, webpage, or document

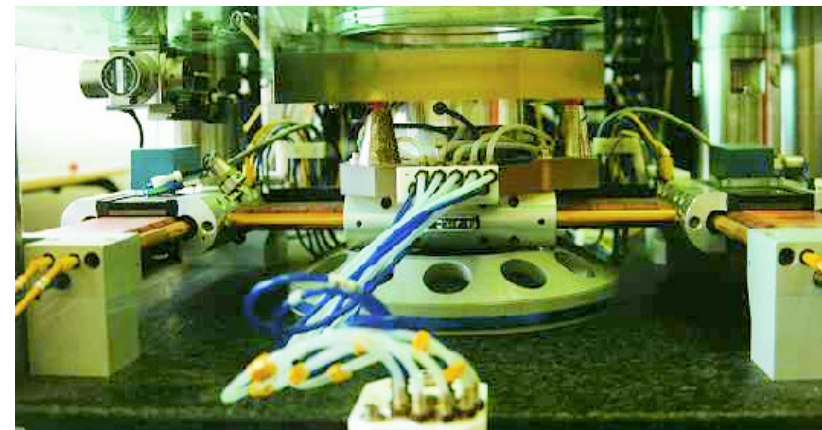
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Identificatie & Regelaar Tuning
Een Stukje Hardheid op de Tafel

Translation: Dutch » English

Identification and Controller Tuning
A Piece of hardness on the Table

- hardness = rigidity, solidity or just hard facts?
- From a PhD student's point of view:
 - Explain yourself in rigorous math
 - Show me your papers
 - I want to see how it works!
 - Where is your thesis?



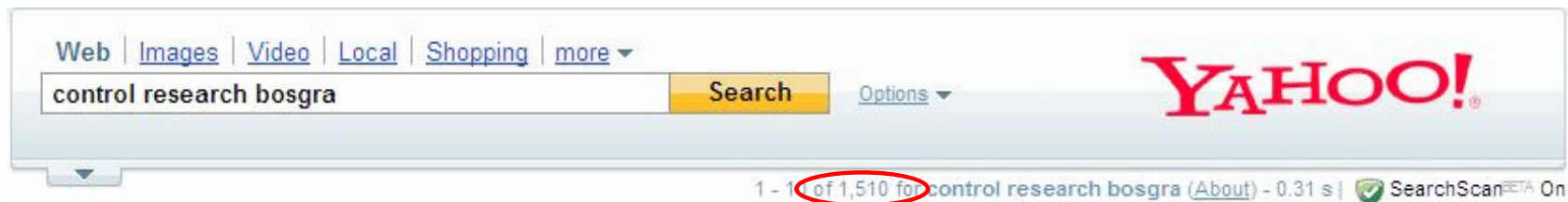
another table...

Frustration of not able to see any things on the table...

- Control: hidden technology
- Algorithms, Embedded, Integrated and Fed Back
- Name `control' itself is ambiguous (common & Kalman)
- A lot of research in many, many journals



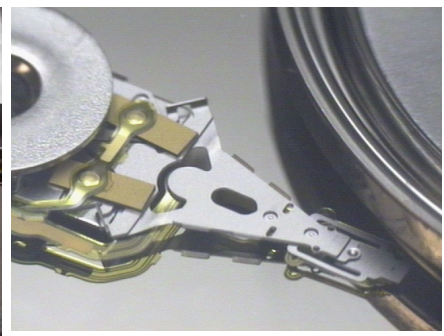
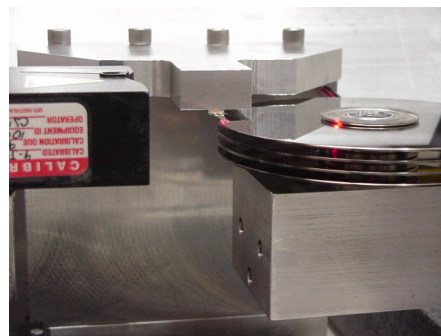
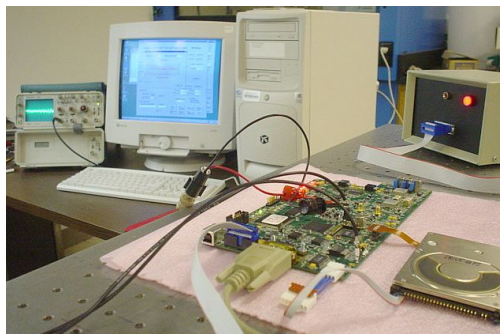
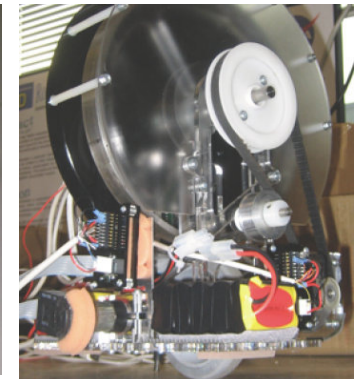
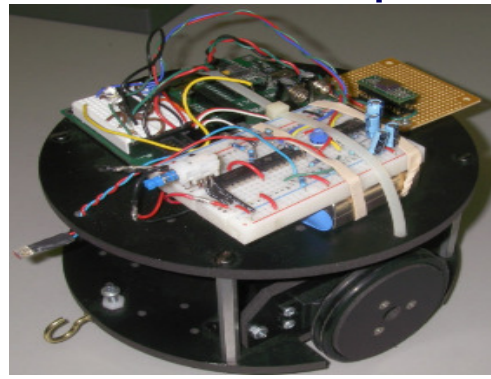
Web [Show options...](#) Results 1 - 10 of about 80,900,000 for control journal. (0.43 seconds)



- Bosgra: creating some order in the chaos!

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- System identification, interaction between data-based modeling and control, identification of LPV systems, adaptive control, motion control.
- Applications include mechanical, servo, and structural systems, including data storage systems (hard disks and tapes) and active noise control.
- Industrial partners includes Seagate, Western Digital, Cymer, Hewlett-Packard, Quantum, Kodak, Vektrex and industrial sponsors via INSIC.

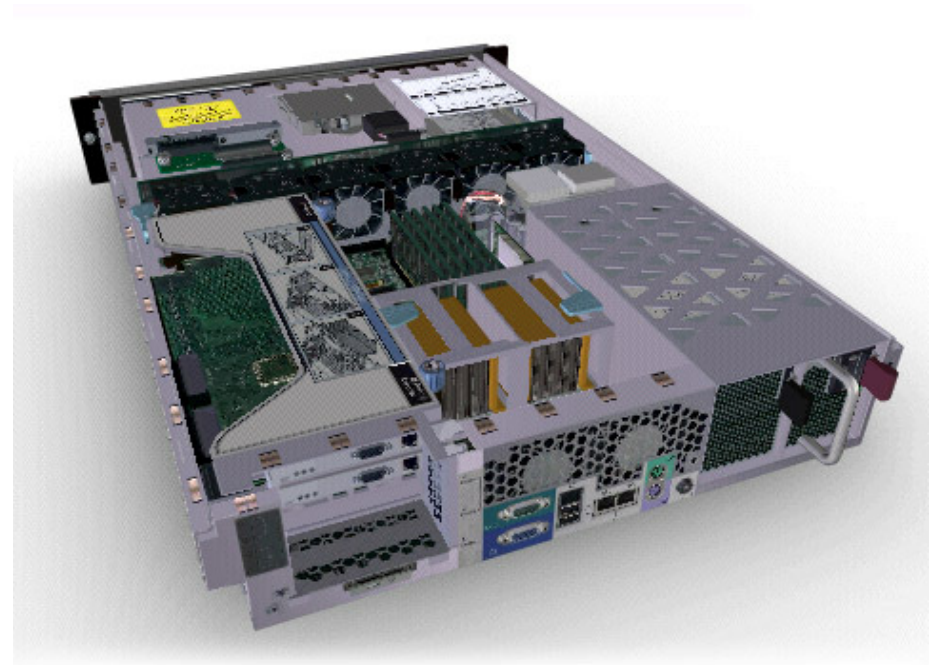
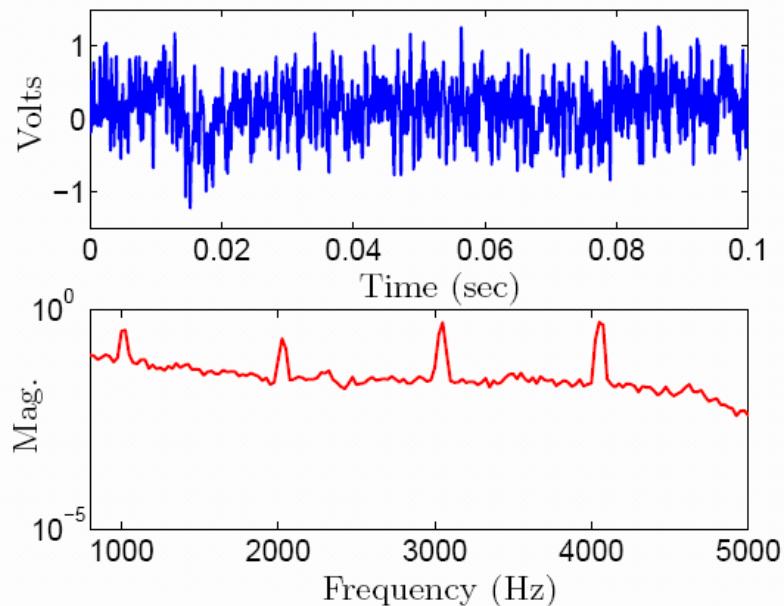


Een Klein Stukje Hardheid op de Tafel: Robust Estimation for Automatic Control Tuning (REACT)

- Motivation & Illustration
- Some Details
 - Plant and Controller perturbation
 - Error signal
 - Variance minimization
 - Stability robustness
- Example & Application

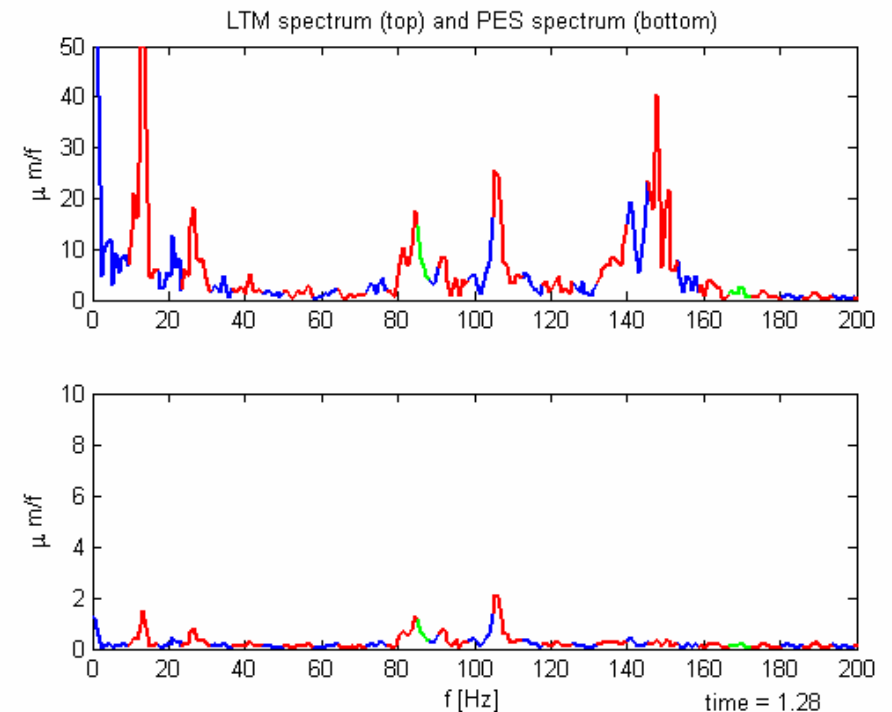
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Application in Active Noise Control of Cooling Fans:



- Blade Pass Frequency (BPF) cause harmonic sound disturbances, along with non-periodic airflow noise
- Speed of fan and BPF not known and vary over time
- HP and Dell especially interested in Active Sound Compensation (ASC) of BPF and 'beating' phenomena

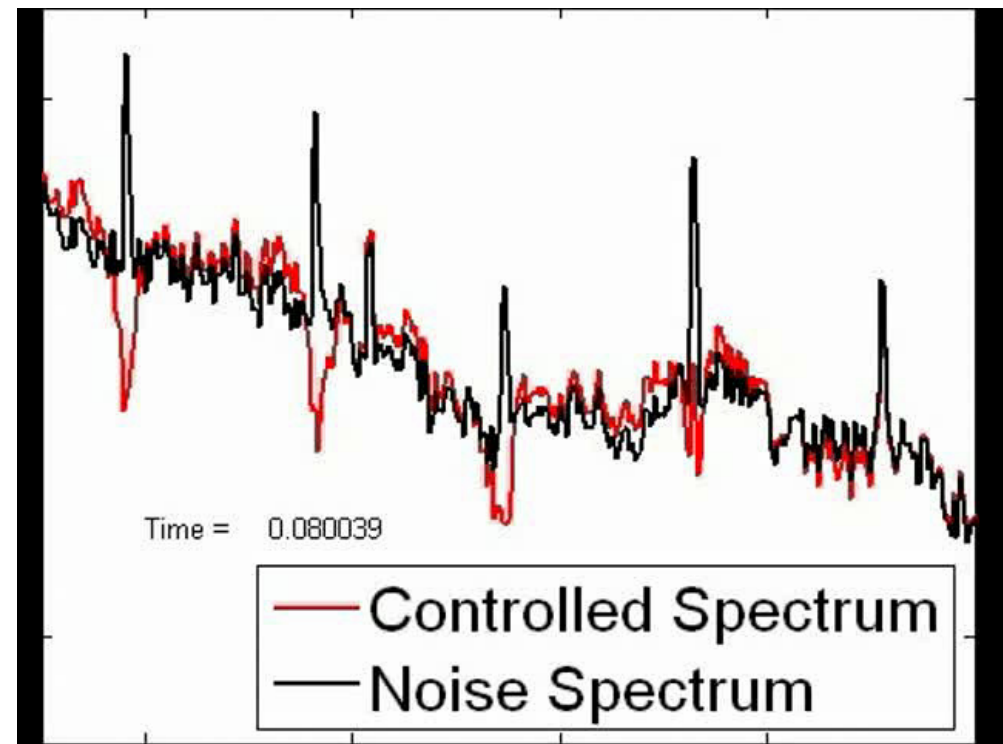
Application in High Density Tape Storage (1/2 height LTO drive):



- Rotation of cartridge reel cause periodic disturbances
- Reel diameter changes over time and tape runs at varying speeds
- Unknown non-periodic disturbance spectra

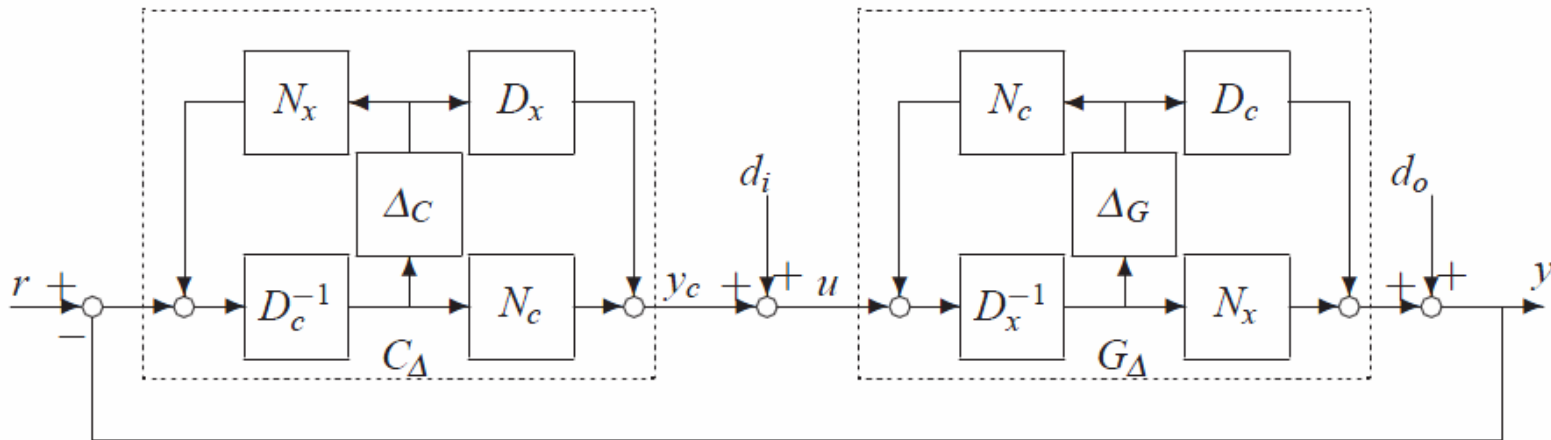
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Demonstration of REACT:



- Double fan contained in box with control baffle that contains speakers and microphones in feedback configuration
- Adaptive tuning of servo controller to cancel harmonics

Consider simultaneous **Plant** and **Controller** perturbation in Youla parametrization:



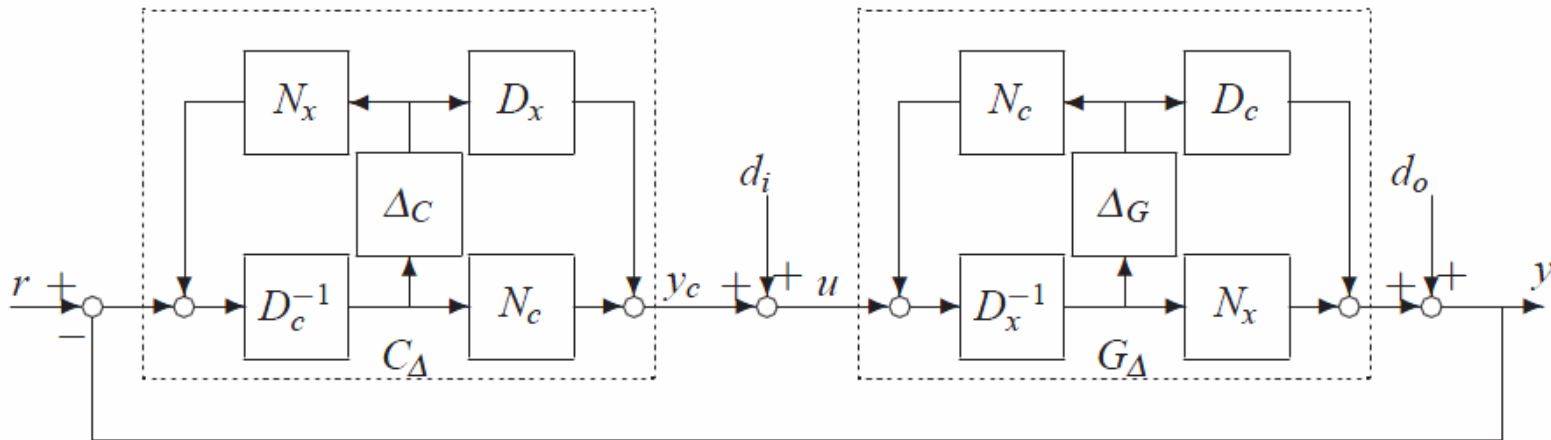
Plant:

$$G_{\Delta} = N_{G_{\Delta}} D_{G_{\Delta}}^{-1} = (N_x + D_c \Delta_G)(D_x - N_c \Delta_G)^{-1}$$

$$\Xi = \{ \Delta : \|\Delta\|_{\infty} < 1/\gamma, \Delta \in \mathcal{RH}_{\infty} \}$$

$$\Pi = \{ P : P = (N_x + D_c \Delta_G)(D_x - N_c \Delta_G)^{-1}, \Delta_G \in \Xi \}$$

Consider simultaneous **Plant** and **Controller** perturbation in Youla parametrization:



Controller: $C_\Delta = N_{C_\Delta} D_{C_\Delta}^{-1} = (N_C + D_x \Delta_C)(D_C - N_x \Delta_C)^{-1}$

$$\Delta_C[u(t)] = \Theta(t)^T \int_0^t (C_D e^{A_D(t-\tau)} B_D + D_D) u(\tau) d\tau$$

$$= \Theta(t)^T (\mathcal{D}(t) * u(t)), \quad \mathcal{D}^T = \left[\mathbf{I} \left(\frac{s-p_0}{s+p_0} \right) \mathbf{I} \left(\frac{s-p_0}{s+p_0} \right)^2 \dots \mathbf{I} \left(\frac{s-p_0}{s+p_0} \right)^{n_\theta} \right]$$

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At this point, we will introduce two parameters: θ and Ψ

- Needed to separate optimization problem from control problem
- $\Delta_C(\theta)$: controller perturbation **used in optimization**
- $\Delta_C(\Psi)$: controller perturbation **used in feedback**

Benefit from Youla parametrization and parameter separation:

$$\begin{aligned}
 y &= (I + G_\Delta C_\Delta)^{-1} d_o + G_\Delta (I + C_\Delta G_\Delta)^{-1} d_i \\
 &= (I + G_\Delta C_\Delta)^{-1} d_o + (I + G_\Delta C_\Delta)^{-1} G_\Delta d_i \\
 &= D_{C_\Delta} \tilde{\Lambda}^{-1} \tilde{D}_{G_\Delta} (d_o + G_\Delta d_i),
 \end{aligned}$$

can be written as an *error signal* based on $y(t)$ and $y_c(t)$:

$$\begin{aligned}
 \varepsilon(t, \theta, \psi) &:= (D_c(t) - N_x(t) \Delta_C(t, \theta)) * \eta(t, \psi) \\
 \eta(t, \psi) &= \Lambda_o^{-1}(t) * (\tilde{D}_x(t) * y(t) - \tilde{N}_x(t) * y_c(t, \psi))
 \end{aligned}$$

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To guarantee stability of the feedback system during adaptation, we have the following main result:

With

$$\Xi = \{\Delta : \|\Delta\|_\infty < 1/\gamma, \Delta \in \mathcal{RH}_\infty\}$$

$$\Pi = \{P : P = (N_x + D_c \Delta_G)(D_x - N_c \Delta_G)^{-1}, \Delta_G \in \Xi\}$$

consider the simultaneously perturbed feedback system in which θ in

$$\begin{aligned} \Delta_C[u(t)] &= \Theta(t)^T \int_0^t (C_D e^{A_D(t-\tau)} B_D + D_D) u(\tau) d\tau \\ &= \Theta(t)^T (\mathcal{D}(t) * u(t)), \end{aligned}$$

is replaced by Ψ . If the time-varying matrix $\Psi(t)$ satisfies

$$\|\Psi(t)\|_2^2 \leq \frac{\gamma^2}{\|\mathcal{D}\|_\infty} \quad \forall t$$

then the feedback system is L2-stable for all $G_\Delta \in \Pi$

How can we use this during optimization to guarantee stability robustness?

Theorem *Suppose that $\|\Delta_G\|_\infty < 1/\gamma$, and the frozen time system Δ_C satisfies $\|\Delta_C(\Psi)\|_\infty \leq \gamma(1 - \delta)$ for each $t \geq 0$ and for some $0 < \delta < 1$, and that $\sup_{t \geq 0} \|\Psi(t)\| < \infty$. Then there exists an $\varepsilon > 0$ such that the feedback system of G_Δ and C_Δ is stable if $\sup_{t \geq 0} \|\dot{\Psi}(t)\| \leq \varepsilon$.*

- Restrict “size” of controller perturbation due to model uncertainty, and
- Restrict “change” in controller parameter update:

$$\dot{\theta} = \mu r(t, \psi) - \mu \Phi(t, \psi) \Phi(t, \psi)^T \theta$$

$$\dot{\psi} = \text{Proj}_{\psi \in \mathcal{S}} \left(-\lambda \frac{\psi - \theta}{1 + \|\psi - \theta\|} \right), \quad \mathcal{S} = \left\{ \psi : \|\Psi\|_2 \leq \gamma / \sqrt{\|D\|_\infty} \right\}$$

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$G(q)$ discrete-time ZOH equivalent of:

$$G(s) = \frac{K \omega_1^2 \omega_2^2}{(s^2 + 2\beta_1 \omega_1 s + \omega_1^2)(s^2 + 2\beta_2 \omega_2 s + \omega_2^2)}$$

Resulting signals with $C(q)$:

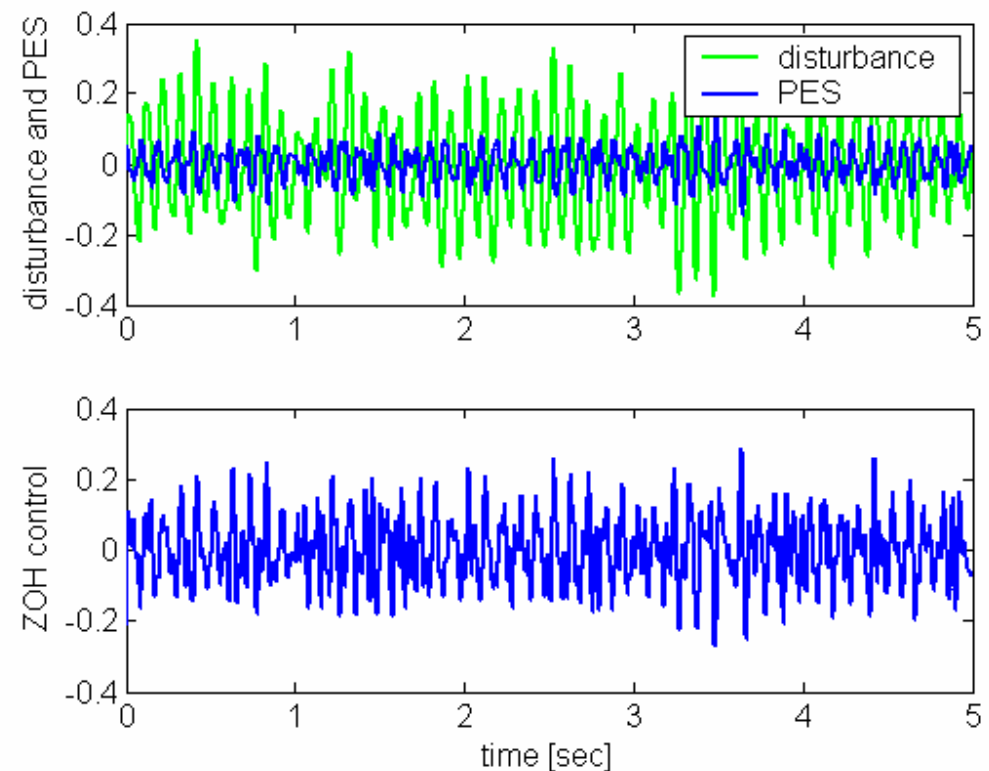
controlled by simple PD controller:

$$C(q) = 10 \cdot \frac{q - 0.995}{q - 0.95}$$

Now subjected to disturbance:

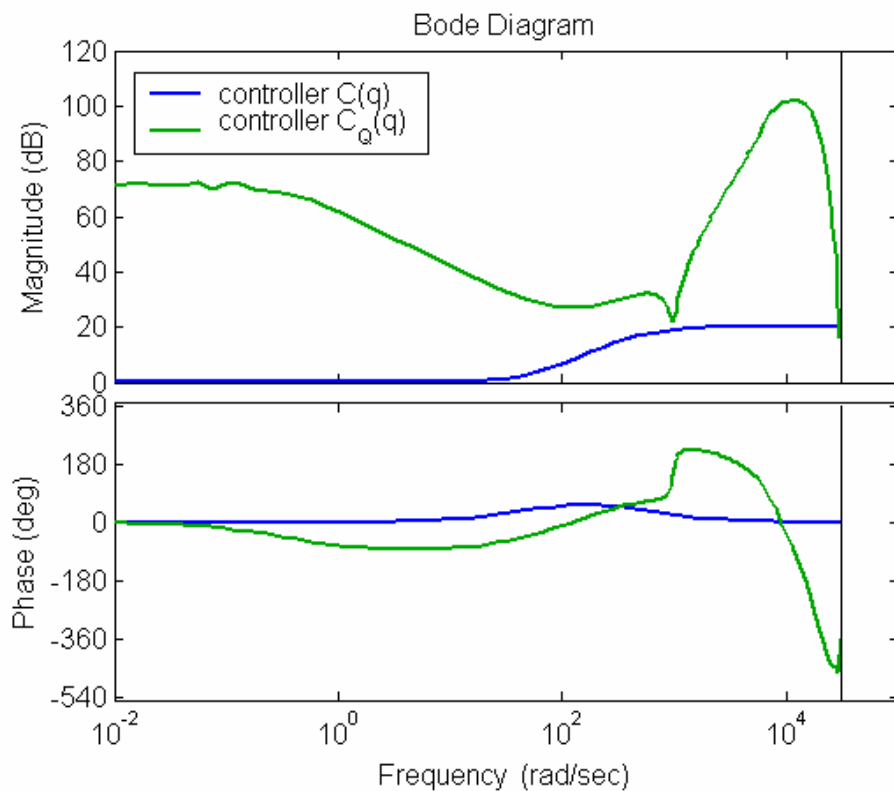
$$d(t) = L(q)\varepsilon(t) + 0.1\sin(2\pi \cdot 10t)$$

where $L(q)$ is a *low pass* filter and $e(t)$ is white noise.

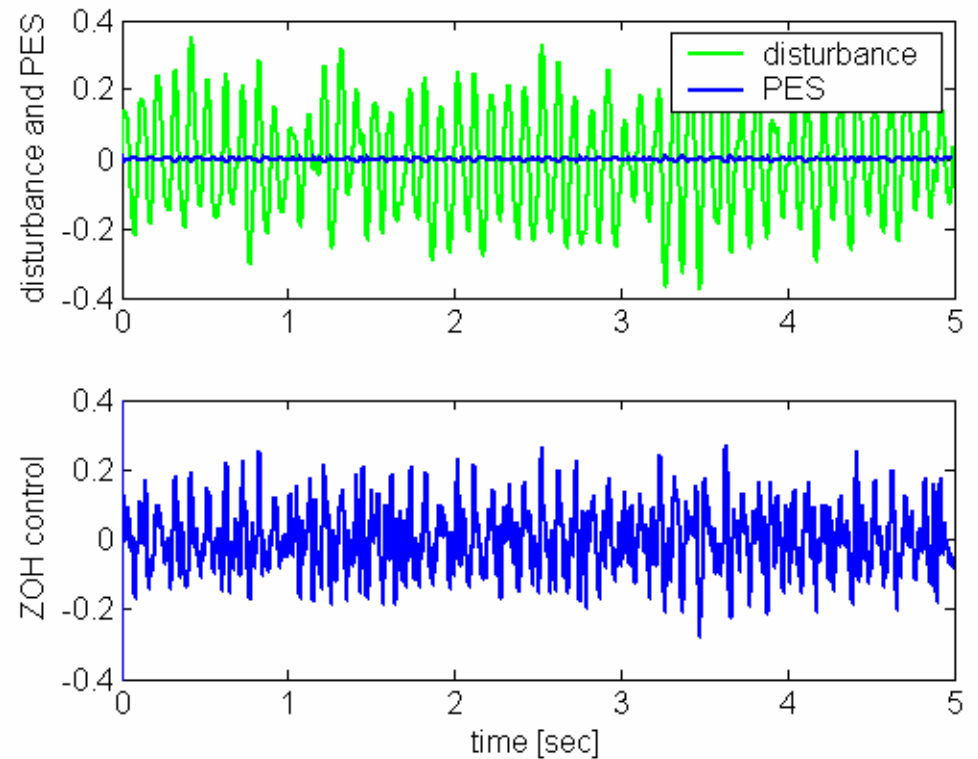


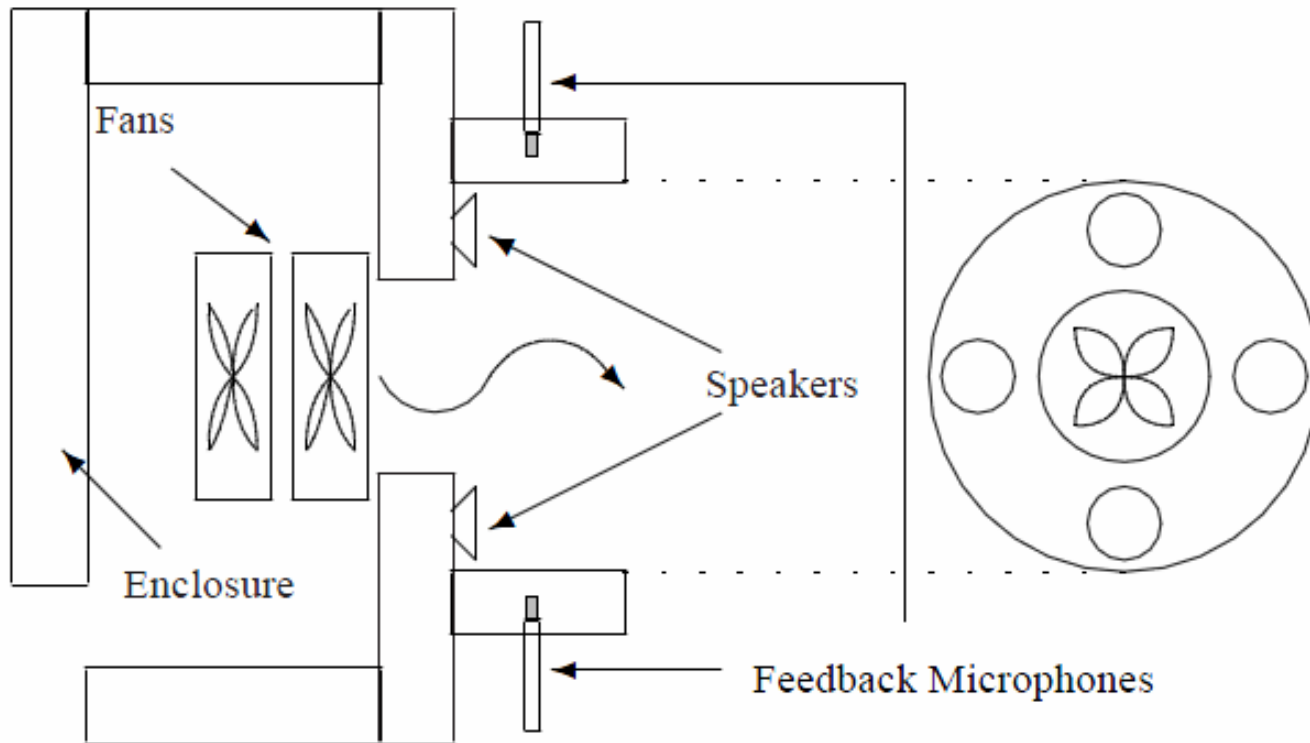
Running REACT to adapt controller with $\Delta_c(q) = 10^{\text{th}}$ order FIR

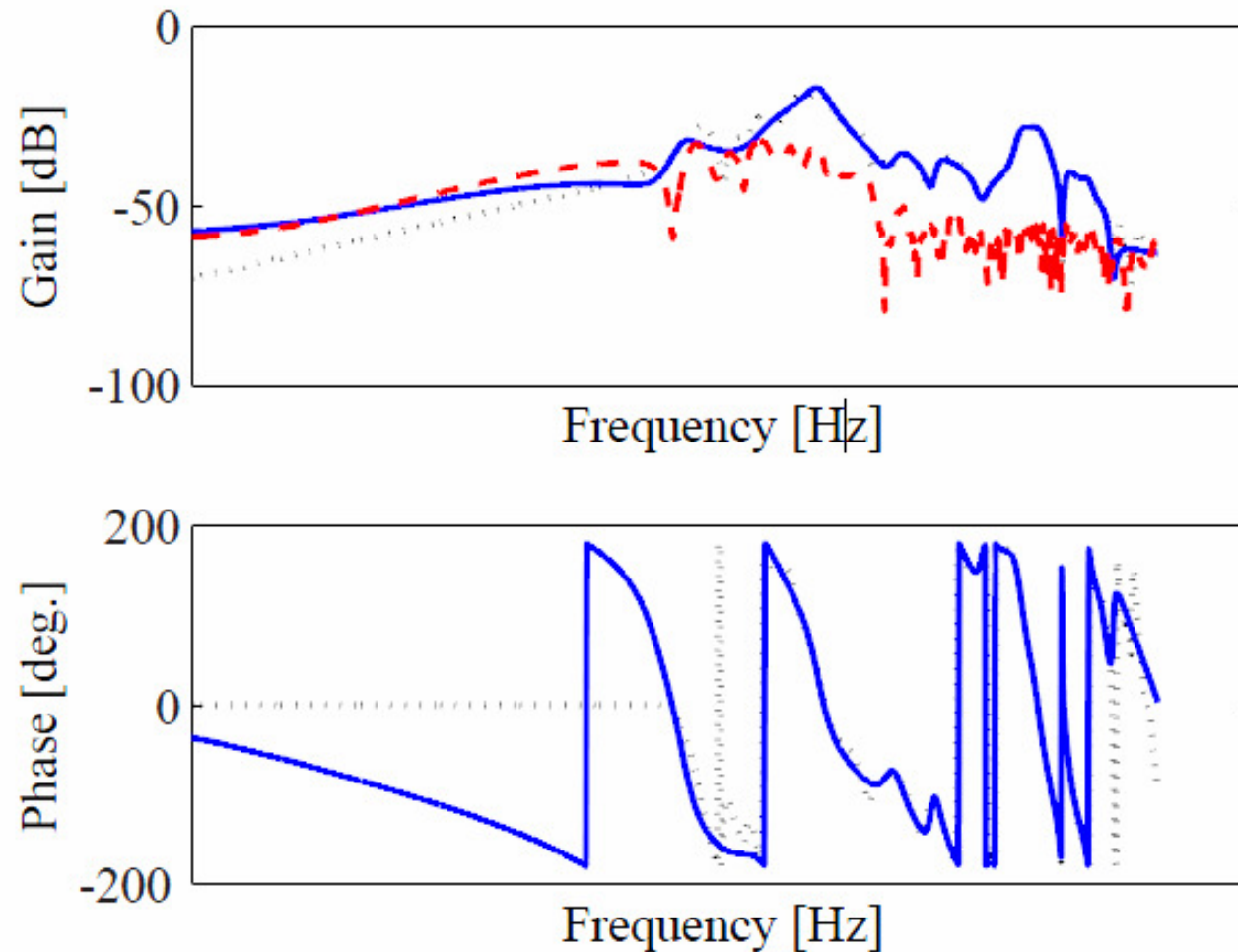
Adaptation of controller:



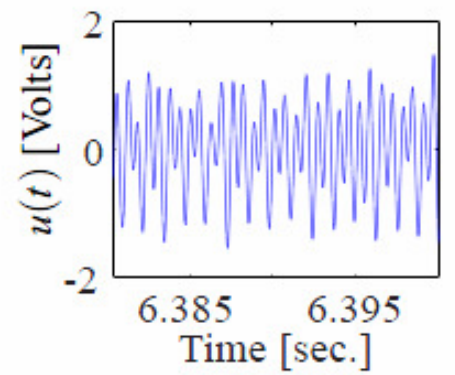
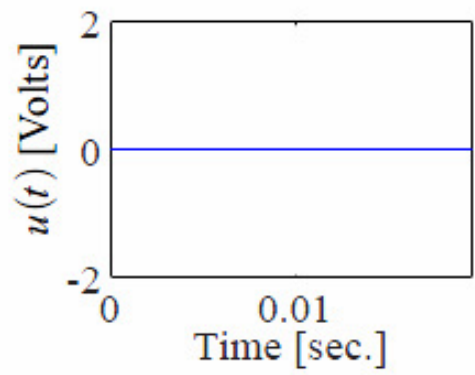
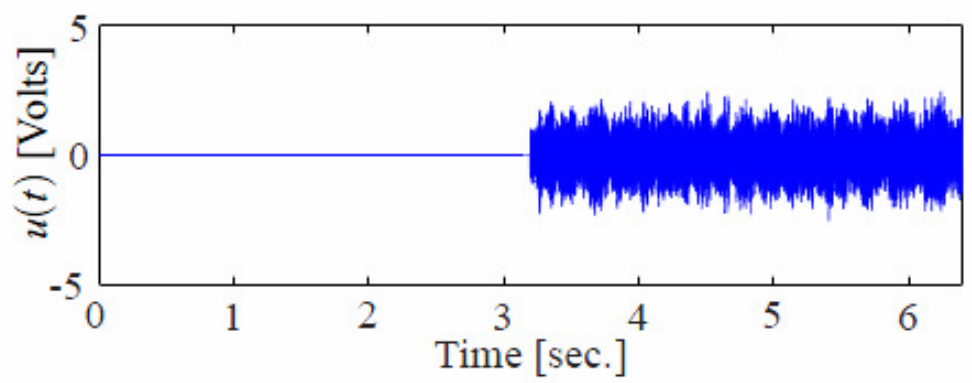
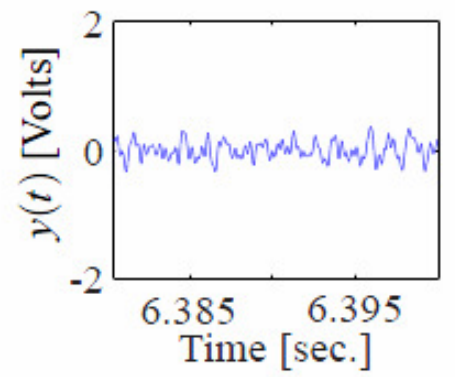
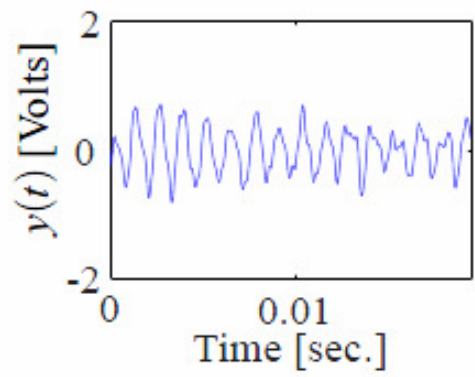
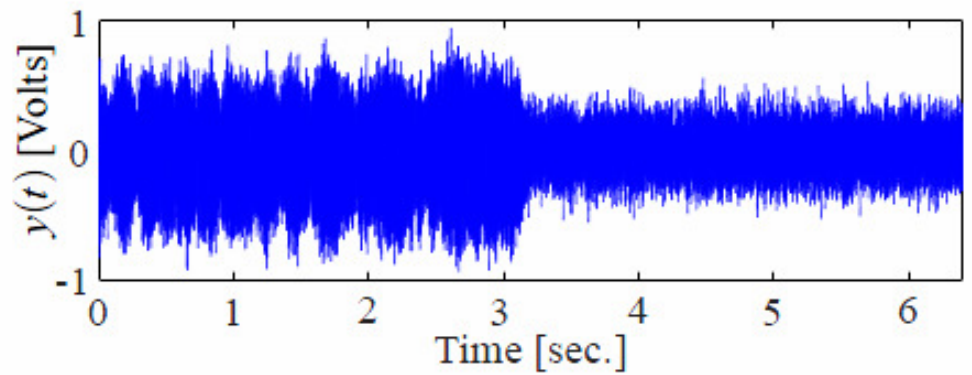
Resulting signals with $C_{\Delta}(q)$:

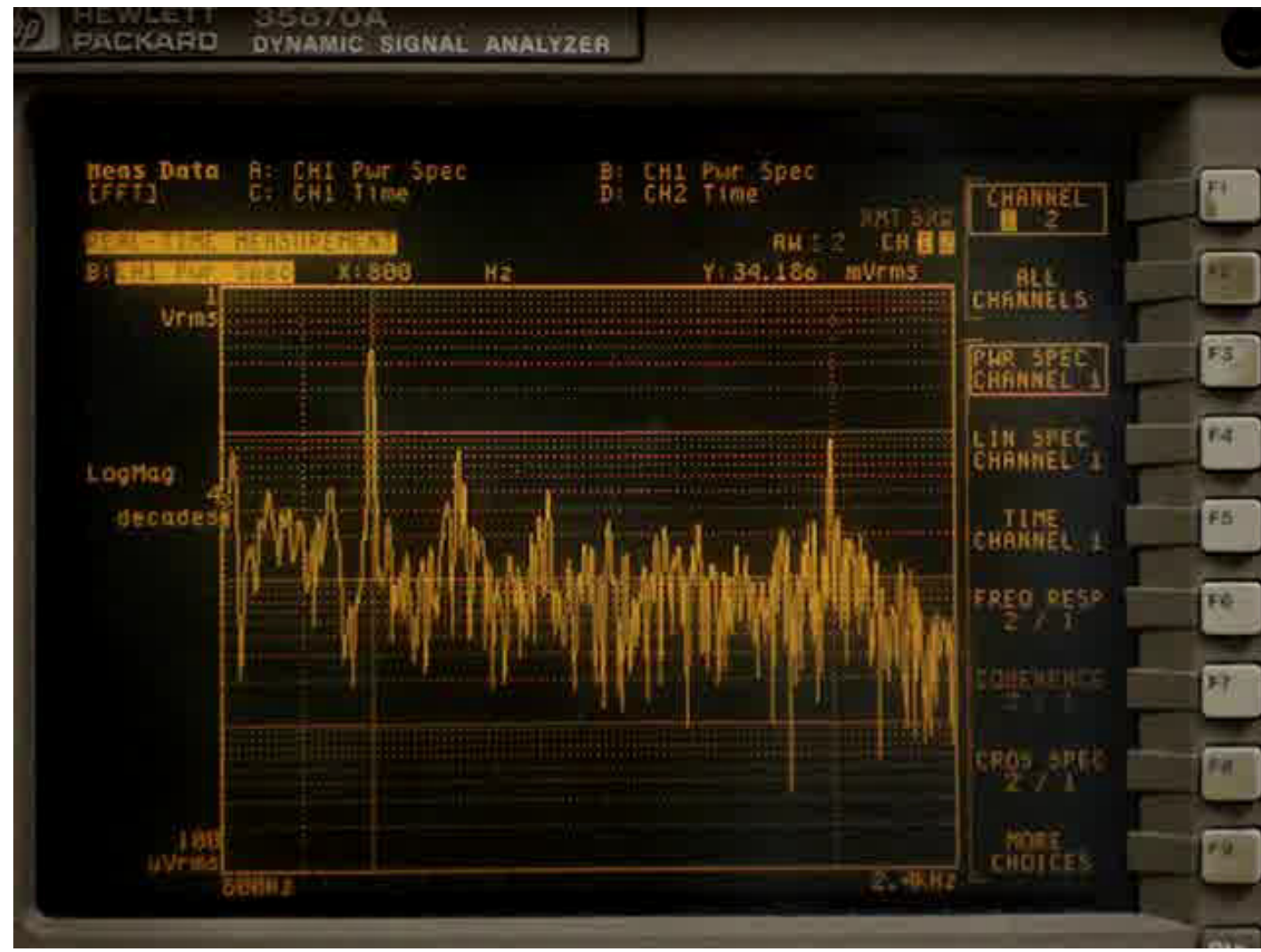






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■ Some Hard Facts:

- Double-Youla parameterization can be used to **recast the robust tuning** of a feedback controller **as a robust estimation problem**
- Robust estimation is obtained by **constraining size and change in the parameter estimates** so that feedback stability will be maintained during controller tuning in the presence of plant uncertainty

■ Some Fun Facts:

- Applied to ANC system and TAPE servo system by *Charles Kinney*
- Adjust *existing* feedback based on the disturbances observed
- Model uncertainty *limits* achievable tuning performance

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- Desire to see/share the same enthusiasm and devotion:
 - Control background: combine abstraction with motivating applications
 - Care about students & listen to what they say (TUDelta.27)
 - On vacation/trip: copy a whole bunch off papers
 - Challenge bureaucracy! Perhaps because we like to be in control?
- But make it fun at the same time:
 - Sense of humor and colorful people in a group
 - Spend some time in the lab
 - Get that bottle of wine from the other table
- Proof of devotion:
 - DISC, Leermesterprijs in 2007 and > 450 students and > 60 PhD
 - Still, visit your PhD student in San Diego and make sure he finishes!
 - Challenge retirement! And enjoy your presence in controls...