

Modeling & Control of Hybrid Systems

Chapter 6 – Optimization-Based Control

Overview

1. Optimal control of hybrid systems
2. MPC for MLD and PWA systems
3. MPC for MMPS and continuous PWA systems
4. Game-theoretic approaches

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1.1 Optimal control for hybrid manufacturing systems

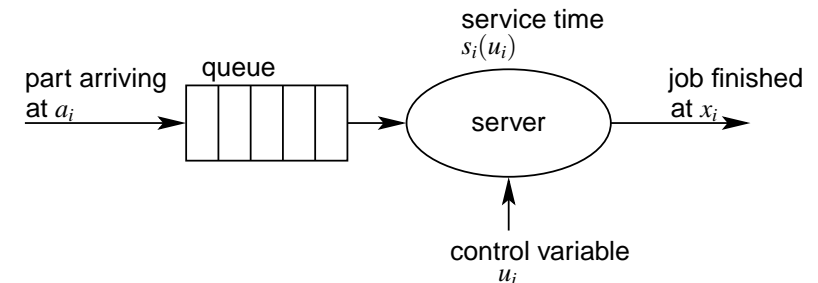
- Manufacturing system: jobs move through network of work centers
 - Jobs have
 - *temporal state* (event-driven): waiting time, departure time, ...
 - *physical state* (time-driven): temperature, size, weight, chemical composition, ...
 - Trade-off between
 - temporal requirements on job completion times
 - physical requirements on quality of completed jobs
- assume higher quality \rightarrow longer processing times

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1. Optimal control of a class of hybrid systems

1. Optimal control for hybrid manufacturing systems
2. Example
3. Optimality conditions

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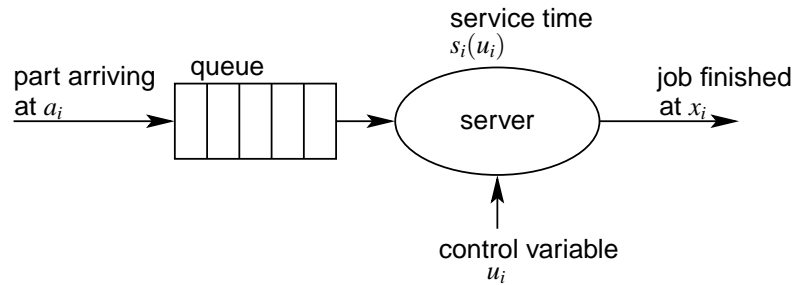


- Single-stage, single-server queueing system
- N jobs (each job corresponds to mode)
- Buffer with capacity $> N$
- As job i is processed, physical state z_i evolves according to

$$\dot{z}_i = g_i(z_i, u_i, t) \quad \text{with } z_i(\tau_i) = \zeta_i$$

with τ_i time instant at which processing begins

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- Control variable u_i is used to attain final desired physical state:
If $s_i(u_i)$ is *service time* and $\Gamma_i(u_i)$ is target quality set, then

$$s_i(u_i) = \min\{t \geq 0 \mid z_i(\tau_i + t) \in \Gamma_i(u_i)\}$$

- *Temporal state* x_i represents time when job is completed:
If a_i is arrival time of job i , then

$$x_i = \max(x_{i-1}, a_i) + s_i(u_i) \quad (\text{Lindley equation}) \quad \text{hs_opt_ctrl.5}$$

1.2 Example

- Steel heating/annealing manufacturing processes
- Involves slowly heating and cooling strips to some desired temperatures
- Higher level controller determines furnace reference temperature + amount of time strip is held in furnace
- Physical state z_i represents temperature and depends on *line speed* u_i and *furnace reference temperature* F_i :

$$\dot{z}_i(t) = -\frac{F_i - z_i(t_0)}{L}u_i + K_s(F_i^4 - z_i^4(t)) \quad \text{for } t \geq t_0$$

- Constraint: $u_{\min} \leq u_i \leq u_{\max}$

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Optimal control for hybrid manufacturing systems (cont.)

Optimal control problem:

$$\min_{u_1, \dots, u_N} J = \sum_{i=1}^N L_i(x_i, u_i)$$

subject to evolution equations for z_i and x_i

where $L(x_i, u_i)$ is cost function associated with job i

→ classical discrete-time optimal control problems except for

- i does not count time steps
→ not really an issue
- max is non-differentiable for $a_i = x_{i-1}$
→ prevents use of standard gradient-based techniques
→ use non-differentiable calculus, generalized gradient

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1.2 Example (continued)

- Temporal state:

x_i : time when job starts processing at furnace, i.e.
strip completely inside furnace

y_i : time when job completes processing

$$x_i = \max(a_i, x_{i-1}) + s_1(u_i) \quad \text{and} \quad y_i = x_i + s_2(u_i)$$

with $s_1(u_i)$ elapsed time for whole body of strip to enter furnace (is dependent on length of strip),
and $s_2(u_i)$ processing time for each point of strip to run through furnace (is dependent on length of furnace)

- Two control objectives:

1. reduce temperature errors w.r.t. furnace reference temperature
2. reduce entire processing time

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1.2 Example (continued)

- Thus, optimal control problem is

$$\min_{u_1, \dots, u_N} J = \sum_{i=1}^N (\theta(u_i) + \phi(y_i))$$

subject to physical and temporal evolution equations

with

- $\phi(y_i)$ cost related to jobs departing at time y_i
e.g., $\phi(y_i) = (y_i - d_i)^2$, with d_i due date
→ penalizes tardiness, and early completion (inventory cost)
- $\theta(u_i)$ penalizes deviation from reference temperature F_i :

$$\theta(u_i) = |F_i - z_i(L/u_i)|^2 + \beta \int_0^{L/u_i} (F_i - z_i(t))^2 dt$$

where L/u_i is time each point of strip stays in furnace

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1.3 Optimality conditions (continued)

- Results in

- Stationarity condition: $\frac{\partial L_i(x_i, u_i)}{\partial u_i} + \lambda_i \frac{ds_i(u_i)}{du_i} = 0$
- Temporal state equation: $x_i = \max(x_{i-1}, a_i) + s_i(u_i)i$
with $x_0 = -\infty$
- Co-state equation: $\lambda_i = \frac{\partial L_i(x_i, u_i)}{\partial x_i} + \lambda_{i+1} \frac{d \max(x_i, a_{i+1})}{dx_i}$ with final boundary condition

$$\lambda_N = \frac{\partial L_N(x_N, u_N)}{\partial x_N}$$

- Defines *two-point boundary-value problem* (TPBVP)

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1.3 Optimality conditions

- Define augmented cost:

$$\bar{J}(x, \lambda, u) = \sum_{i=1}^N (L_i(x_i, u_i) + \lambda_i(\max(x_{i-1}, a_i) + s_i(u_i) - x_i))$$

where λ is co-state

- Assumption: costs L_i and s_i are continuously differentiable
- Ignoring non-differentiabilities associated with \max , standard first-order necessary conditions for optimality require

$$\frac{\partial \bar{J}}{\partial u_i} = 0, \quad \frac{\partial \bar{J}}{\partial \lambda_i} = 0, \quad \frac{\partial \bar{J}}{\partial x_i} = 0 \quad \text{for } i = 1, \dots, N$$

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How to deal with non-differentiability

- \max is Lipschitz continuous + differentiable except for $x_i = a_{i+1}$:

$$\frac{d \max(x_i, a_{i+1})}{dx_i} = \begin{cases} 0 & \text{if } x_i < a_{i+1} \\ 1 & \text{if } x_i > a_{i+1} \end{cases}$$

- Use *generalized gradient*:

Let $f : \mathbb{R}^n \rightarrow \mathbb{R}$ be locally Lipschitz continuous, and let $S(u)$ denote set of all sequences $\{u_m\}_{m=1}^\infty$ that satisfy

- $u_m \rightarrow u$ as $m \rightarrow \infty$
- gradient $\nabla f(u_m)$ exists for all m
- $\lim_{m \rightarrow \infty} \nabla f(u_m) = \phi$ exists

Then *generalized gradient* $\partial f(u)$ is defined as convex hull of all limits ϕ corresponding to some sequence $\{u_m\}_{m=1}^\infty$ in $S(u)$

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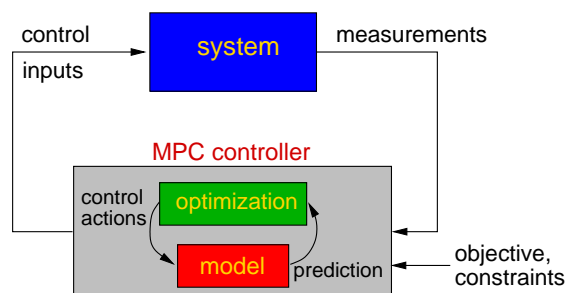
How to deal with non-differentiability (continued)

- Properties of generalized gradient:
 - if f is continuously differentiable in some open set containing u , then $\partial f(u) = \{\nabla f(u)\}$
 - if u is local minimum, then $0 \in \partial f(u)$
 - this becomes first-order optimality condition in non-smooth optimization
- See lecture notes for computation of $\partial \bar{J}$
- Note: presence of idle period results in decoupling

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2.1 Model predictive control (MPC)

- Very popular in process industry
- Model-based
- Easy to tune
- Multi-input multi-output (MIMO)
- Allows constraints on inputs and outputs
- Adaptive / receding horizon
- Uses on-line optimization



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2. MPC for MLD systems

1. Model predictive control (MPC)
2. MPC for MLD and PWA systems

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MPC (continued)

At sample step k :

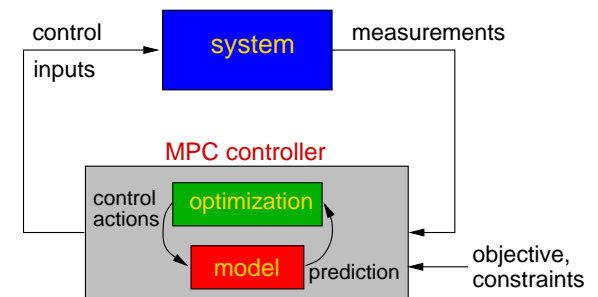
- Use model to predict system output over prediction period $[k, k + N_p]$ for given input sequence $u(k), \dots, u(k + N_p - 1)$

N_p : prediction horizon

$$\tilde{u}(k) = [u^T(k) \dots u^T(k + N_p - 1)]^T$$

- Define performance criterion $J(k)$ over $[k, k + N_p]$, e.g.,
 $J(k) = \text{tracking error} + \lambda \cdot \text{input effort/energy}$

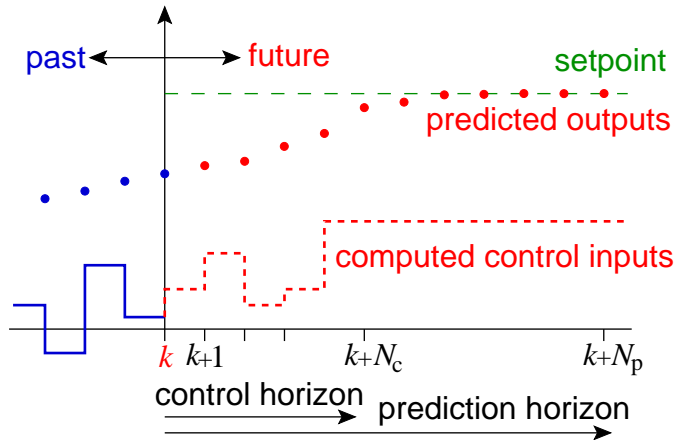
- Constraints on u, x, y



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MPC problem

- Find at sample step k input sequence $\tilde{u}(k)$ that minimizes $J(k)$ subject to system equations + constraints



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MPC problem (continued)

Receding horizon principle:

- Compute optimal input sequence $\tilde{u}(k)$
- Implement only first sample $u(k)$
- Update model & shift interval
- Restart optimization

Extra condition to reduce computational complexity:
control horizon N_c

$$u(k+j) = u(k+N_c-1) \quad \text{for } j = N_c, \dots, N_p-1$$

→ smoother controller signal & stabilizing effect

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2.2 MPC for MLD systems

- Consider MLD system:

$$x(k+1) = Ax(k) + B_1u(k) + B_2\delta(k) + B_3z(k)$$

$$y(k) = Cx(k) + D_1u(k) + D_2\delta(k) + D_3z(k)$$

$$E_1x(k) + E_2u(k) + E_3\delta(k) + E_4z(k) \leq g_5,$$
- $x(k) = [x_r^\top(k) \ x_b^\top(k)]^\top$ with $x_r(k)$ real-valued, $x_b(k)$ boolean
 $z(k)$: real-valued auxiliary variables
 $\delta(k)$: boolean auxiliary variables
- Consider equilibrium state/input/output $(x_{eq}, u_{eq}, y_{eq}) \rightarrow (\delta_{eq}, z_{eq})$
- $\hat{x}(k+j|k)$: estimate of x at sample step $k+j$ based on information available at sample step k

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2.2 MPC for MLD systems (continued)

- Stabilize system to equilibrium state:

$$J(k) = \sum_{j=1}^{N_p} \|\hat{x}(k+j|k) - x_{eq}\|_{Q_x}^2 + \|u(k+j-1) - u_{eq}\|_{Q_u}^2 + \|\hat{y}(k+j|k) - y_{eq}\|_{Q_y}^2 + \|\hat{\delta}(k+j-1|k) - \delta_{eq}\|_{Q_\delta}^2 + \|\hat{z}(k+j-1|k) - z_{eq}\|_{Q_z}^2$$

with $Q_{(-)} \geq 0$

- End-point condition: $\hat{x}(k+N_p|k) = x_{eq}$
- Control horizon constraint:
 $u(k+j) = u(k+N_c-1)$ for $j = N_c, \dots, N_p-1$

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2.2 MPC for MLD systems (continued)

- **Property:**

If feasible solution exists for $x(0)$, then MPC input stabilizes system, i.e.,

$$\begin{aligned} \lim_{k \rightarrow \infty} x(k) &= x_{\text{eq}} & \lim_{k \rightarrow \infty} \|y(k) - y_{\text{eq}}\|_{Q_y} &= 0 & \lim_{k \rightarrow \infty} \|z(k) - z_{\text{eq}}\|_{Q_z} &= 0 \\ \lim_{k \rightarrow \infty} u(k) &= u_{\text{eq}} & \lim_{k \rightarrow \infty} \|\delta(k) - \delta_{\text{eq}}\|_{Q_\delta} &= 0 \end{aligned}$$

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Algorithms for MLD-MPC (continued)

- MIQP = NP-hard
- For small-sized problems: cutting plane methods, decomposition methods, logic-based methods, *branch-and-bound* methods (tree search)
- Software:
 - Multi-Parametric Toolbox (MPT) : <http://control.ee.ethz.ch/~mpt/>
 - Hybrid toolbox : <http://www.dii.unisi.it/hybrid/toolbox/>
 - TOMLAB, CPLEX, Xpress
 - NAG, Matlab NAG Toolbox

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Algorithms for MLD-MPC

→ **mixed-integer quadratic programming** (MIQP)

- Successive substitution of system equations:
 - $\hat{x}(k+j|k)$ is linear function of $x(k)$, \tilde{u} , $\tilde{\delta}$ and \tilde{z}
 - Also holds for $\hat{y}(k+j|k)$
- Define $\tilde{V}(k) = [\tilde{u}^\top(k) \ \tilde{\delta}^\top(k) \ \tilde{z}^\top(k)]^\top$
 - contains both real-valued and integer-valued components
- Results in

$$\min_{\tilde{V}(k)} \tilde{V}^\top(k) S_1 \tilde{V}(k) + 2(S_2 + x^\top(k) S_3) \tilde{V}(k) \quad (1)$$

$$\text{subject to } F_1 \tilde{V}(k) \leq F_2 + F_3 x(k) \quad , \quad (2)$$

= MIQP problem

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3. MPC for continuous PWA systems

1. Equivalence of continuous PWA and MMPS systems
2. Canonical forms of MMPS functions
3. Model predictive control for MMPS systems
4. Algorithms for MMPS-MPC
5. Example

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3.1 Equivalence of continuous PWA and MMPS systems

PWA systems

- Continuous PWA function $f : \mathbb{R}^n \rightarrow \mathbb{R}$:
 - domain space divided into polyhedral regions $R_{(1)}, \dots, R_{(N)}$
 - in each region $R_{(i)}$ f can be expressed as

$$f(x) = \alpha_{(i)}^T x + \beta_{(i)}$$

- f is continuous over border of any two regions
- Continuous PWA system:

$$\begin{aligned} x(k) &= \mathcal{P}_x(x(k-1), u(k)) \\ y(k) &= \mathcal{P}_y(x(k), u(k)) \end{aligned}$$

with $\mathcal{P}_x, \mathcal{P}_y$ vector-valued continuous PWA functions

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PWA systems (cont.)

- Note: continuous PWA model can be used as approximation of general nonlinear continuous state space model

$$\begin{aligned} x(k) &= \mathcal{N}_x(x(k-1), u(k)) \\ y(k) &= \mathcal{N}_y(x(k), u(k)) \end{aligned}$$

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Max-min-plus-scaling (MMPS) systems

- MMPS function f is constructed recursively:

$$f := x_i | \alpha | \max(f_k, f_l) | \min(f_k, f_l) | f_k + f_l | \beta f_k$$

with f_k, f_l again MMPS functions

- Examples:

$$\begin{aligned} &* 5x_1 - \max(x_2 + x_3, 5x_1 - 2x_2) \\ &* \max(x_1, \min(x_2, x_3)) + \max(x_2 - 8x_3 + \min(x_1, 5x_2), -7x_1) \end{aligned}$$

- Note: MMPS function is continuous

- MMPS system:

$$\begin{aligned} x(k) &= \mathcal{M}_x(x(k-1), u(k)) \\ y(k) &= \mathcal{M}_y(x(k), u(k)) \end{aligned}$$

with $\mathcal{M}_x, \mathcal{M}_y$ vector-valued MMPS functions

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Equivalence of continuous PWA and MMPS systems

- Previous result: (General) PWA systems are equivalent to *constrained* MMPS systems
- Any MMPS function is also continuous PWA
- A continuous PWA function f can be rewritten as

$$f = \max_j \min_i (\alpha_i^T x + \beta_i)$$

→ f is also MMPS function

- So classes of continuous PWA functions and MMPS functions coincide

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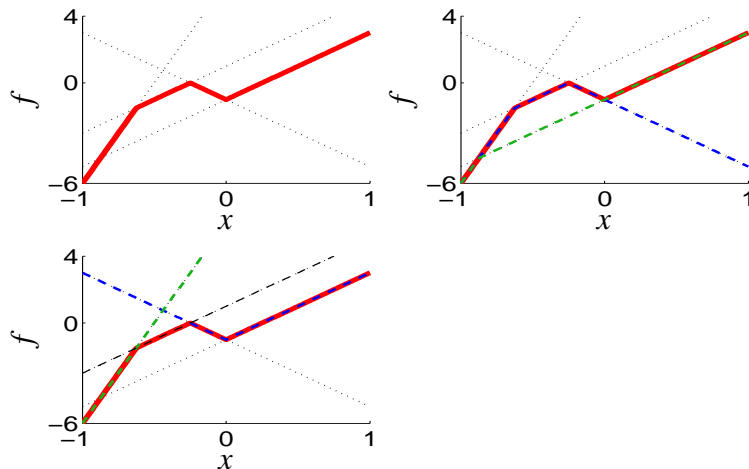
Equivalence of continuous PWA and MMPS systems (cont.)

- Continuous PWA systems and MMPS systems are equivalent:
 - for given continuous PWA model there exists MMPS model (and vice versa) such that input-output behaviors coincide
 - ⇒ use properties & techniques from **continuous** PWA systems for MMPS systems and vice versa

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Example

$$\begin{aligned}
 f(x) &= \min(8x + 6, 1) - 2 \max(\min(2x + 1, 1 - 2x), -2x) \\
 &= \max(\min(12x + 6, 4x + 1, -4x - 1), \min(12x + 6, 4x - 1)) \\
 &= \min(\max(4x - 1, -4x - 1), 12x + 6, 4x + 1)
 \end{aligned}$$



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3.2 Canonical forms of MMPS functions

- Any MMPS function $f : \mathbb{R}^n \rightarrow \mathbb{R}$ can be rewritten into min-max canonical form

$$f = \min_i \max_j (\alpha_{(i,j)}^T x + \beta_{(i,j)})$$

or into max-min canonical form

$$f = \max_i \min_j (\gamma_{(i,j)}^T x + \delta_{(i,j)})$$

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3.3 MPC for MMPS systems

- Use MMPS model

$$\begin{aligned}
 x(k) &= \mathcal{M}_x(x(k-1), u(k)) \\
 y(k) &= \mathcal{M}_y(x(k), u(k))
 \end{aligned}$$

as

- model of MMPS system
- equivalent model of continuous PWA system
- approximation of general smooth nonlinear system

- Prediction horizon: N_p
- Estimate $\hat{y}(k+j|k)$ of output at sample step $k+j$:

$$\hat{y}(k+j|k) = F_j(x(k-1), u(k), \dots, u(k+j))$$

→ F_j is MMPS function!

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3.3 MPC for MMPS systems (continued)

- Reference signal: r
- Cost criterion J : **reference tracking** (J_{out}) vs **control effort** (J_{in}):

$$J(k) = J_{\text{out}}(k) + \lambda J_{\text{in}}(k) \quad \text{with } \lambda > 0$$

- Some possible cost functions:

$$\begin{aligned} J_{\text{out},1}(k) &= \|\tilde{y}(k) - \tilde{r}(k)\|_1 & J_{\text{out},\infty}(k) &= \|\tilde{y}(k) - \tilde{r}(k)\|_\infty \\ J_{\text{in},1}(k) &= \|\tilde{u}(k)\|_1 & J_{\text{in},\infty}(k) &= \|\tilde{u}(k)\|_\infty \end{aligned}$$

with

$$\begin{aligned} \tilde{u}(k) &= [u^T(k) \ \dots \ u^T(k+N_p-1)]^T \\ \tilde{y}(k) &= [\hat{y}^T(k|k) \ \dots \ \hat{y}^T(k+N_p-1|k)]^T \\ \tilde{r}(k) &= [r^T(k) \ \dots \ r^T(k+N_p-1)]^T \end{aligned}$$

Note: $|x| = \max(x, -x) \rightarrow$ cost functions are MMPS functions

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3.3 MPC for MMPS systems (continued)

- Constraints on input and output signals:

$$C_c(k, x(k-1), \tilde{u}(k), \tilde{y}(k)) \geq 0$$

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3.4 Algorithms for MMPS-MPC

- Nonlinear optimization (SQP, ELCP):
→ local minima, excessive computation time
- MPC for mixed logical-dynamical (MLD) systems [Bemporad, Morari]:
→ mixed real-integer quadratic programming problems
- New approach based on canonical forms:
→ set of linear programming problems

LP-based algorithm

Assume: linear (or convex) constraint in $\tilde{u}(k)$

$$P(k)\tilde{u}(k) + q(k) \geq 0$$

Recall: $J(k)$ is MMPS function

$$\begin{aligned} \Rightarrow J(k) &= \max_i (\min_j (\gamma_{(i,j)}^T \tilde{u} + \delta_{(i,j)})) \\ &= \min_i (\max_j (\alpha_{(i,j)}^T \tilde{u} + \beta_{(i,j)})) \end{aligned}$$

$$\begin{aligned} \Rightarrow \min_{\tilde{u}} J(k) &= \min_{\tilde{u}} \min_i (\max_j (\alpha_{(i,j)}^T \tilde{u} + \beta_{(i,j)})) \\ &= \min_i \min_{\tilde{u}} (\underbrace{\max_j (\alpha_{(i,j)}^T \tilde{u} + \beta_{(i,j)})}_{\rightarrow \text{LP!}}) \end{aligned}$$

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LP-based algorithm (cont.)

LP i :

$$\begin{aligned} \min_{\tilde{u}} \quad & t \\ \text{s.t.} \quad & \begin{cases} t \geq \alpha_{(i,j)}^T \tilde{u} + \beta_{(i,j)} & \text{for all } j \\ P\tilde{u} + q \geq 0 \end{cases} \end{aligned}$$

\Rightarrow *set of linear programming problems!*

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3.5 Example (continued)

After substitution:

$$J(k) = \max(\min(t_1, t_2), s_1, s_2, \min(t_3, t_4, t_5), s_3, s_4, s_5)$$

with t_i, s_i affine functions of $x_1(k-1), u(k), u(k+1), r(k)$

Min-max canonical form:

$$J(k) = \min(\max(t_1, t_3, s_1, s_2, s_3, s_4, s_5), \max(t_1, t_4, s_1, s_2, s_3, s_4, s_5), \\ \max(t_1, t_5, s_1, s_2, s_3, s_4, s_5), \max(t_2, t_3, s_1, s_2, s_3, s_4, s_5), \\ \max(t_2, t_4, s_1, s_2, s_3, s_4, s_5), \max(t_2, t_5, s_1, s_2, s_3, s_4, s_5))$$

\rightarrow solve 6 LPs

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3.5 Example

PWA model:

$$y(k) = x(k) = \begin{cases} 0.5x(k-1) + 4u(k) - 1 & \text{if } 0.5x(k-1) + 3.8u(k) \leq 2 \\ 0.2u(k) + 1 & \text{if } 0.5x(k-1) + 3.8u(k) > 2 \end{cases}$$

Equivalent MMPS model:

$$y(k) = x(k) = \min(0.5x(k-1) + 4u(k) - 1, 0.2u(k) + 1)$$

Constraints:

$$-0.2 \leq \Delta u(k) \leq 0.2 \quad \text{and} \quad u(k) \geq 0 \quad \text{for all } k$$

Let $N_c = N_p = 2$ and $J(k) = J_{\text{out},\infty}(k) + \lambda J_{\text{in},1}(k)$

$$= \|\tilde{y}(k) - \tilde{r}(k)\|_{\infty} + \lambda \|\tilde{u}(k)\|_1$$

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3.5 Example (continued)

CPU time for closed-loop MPC over period $[1, 15]$:

Method	CPU time (s)
LP	0.55
SQP	4.90
MLD	2.74
ELCP	198.82

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4. Game-theoretic approaches

- Safety-critical applications such as collision avoidance in free flight or automated highways
 - guarantee safety even in case intentions of other aircraft/vehicle are not known (non-cooperative game)
 - if (partial) communication possible → cooperative game
- Consider continuous-time system

$$\dot{x} = f(x, u, d)$$

with u control inputs (corresponding to 1st player), and d disturbance inputs (corresponding to 2nd player/adversary)

- Assume safety constraints can be represented by set

$$F = \{x \in X \mid k(x) \geq 0\}$$

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Game-theoretic approach (cont.)

- The set

$$\{x \in X \mid \min_{t' \in [t, 0]} J^*(x, t') \geq 0\}$$

contains all states for which system can be forced by control u to remain in safe set F for at least $|t|$ time units, irrespective of disturbance function d

- Value function J^* can be computed using Hamilton-Jacobi equations
 - (numerical) solution of Hamilton-Jacobi equations is tremendous task
 - + approach provides systematic way to check safety properties for continuous-time systems and certain classes of hybrid systems

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Game-theoretic approach

- Let $t \leq 0$ and consider cost function

$$J : X \times \mathcal{U} \times \mathcal{D} \times \mathbb{R}^- \rightarrow \mathbb{R} : (x, u(\cdot), d(\cdot), t) \mapsto k(x(0))$$

where \mathcal{U} and \mathcal{D} denote admissible control and disturbance functions

- Cost is function of final state $x(0)$ only!

→ J is cost associated with trajectory starting at x at time $t \leq 0$ with inputs $u(\cdot)$ and $d(\cdot)$, and ending at time $t = 0$ at the final state $x(0)$

- Define value function

$$J^*(x, t) = \max_{u \in \mathcal{U}} \min_{d \in \mathcal{D}} J(x, u, d, t)$$

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