

Ground Source Heat Pump coupled with Aquifer Thermal Energy Storage System in Building

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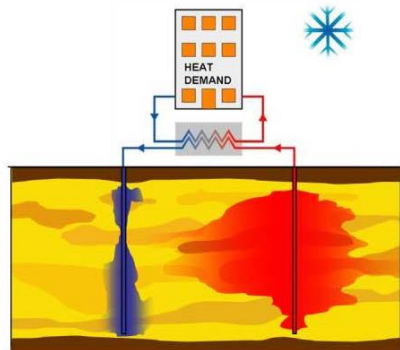


Aquifer Thermal Energy Storage (ATES)

- A large-scale natural subsurface storage for thermal energy
- An innovative method for thermal energy balance in smart grids

Cold season:

- The building requests thermal energy for the heating purpose
- Water is injected into **cold well** and is taken from **warm well**
- The stored water contains **cold** thermal energy for next season

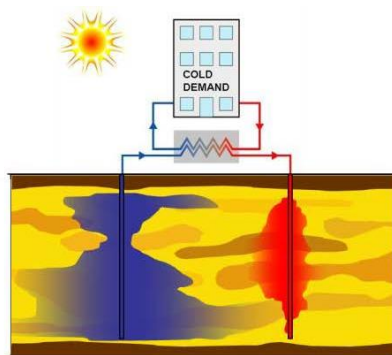


Aquifer Thermal Energy Storage (ATES)

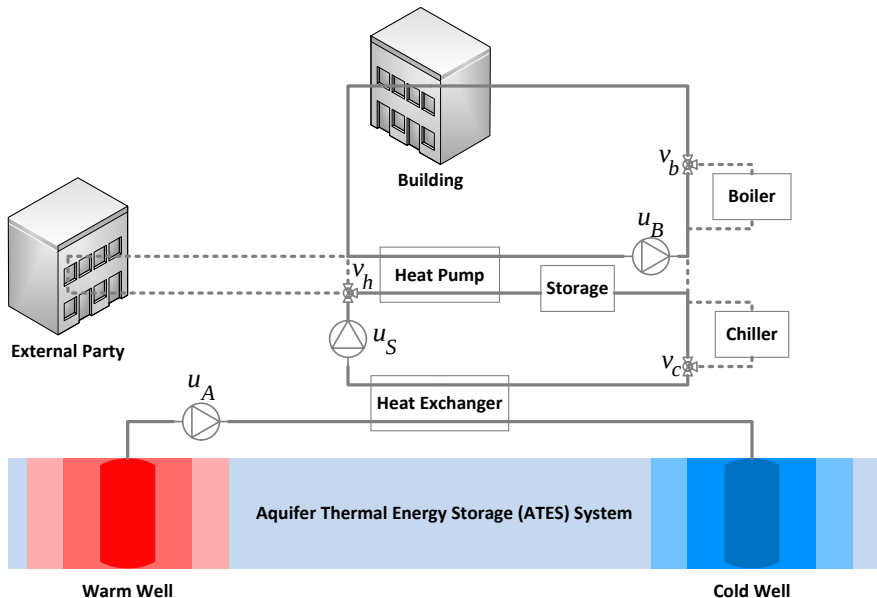
- A large-scale natural subsurface storage for thermal energy
- An innovative method for thermal energy balance in smart grids

Warm season:

- The building requests thermal energy for the cooling purpose
- Water is injected into **warm well** and is taken from **cold well**
- The stored water contains **warm** thermal energy for next season



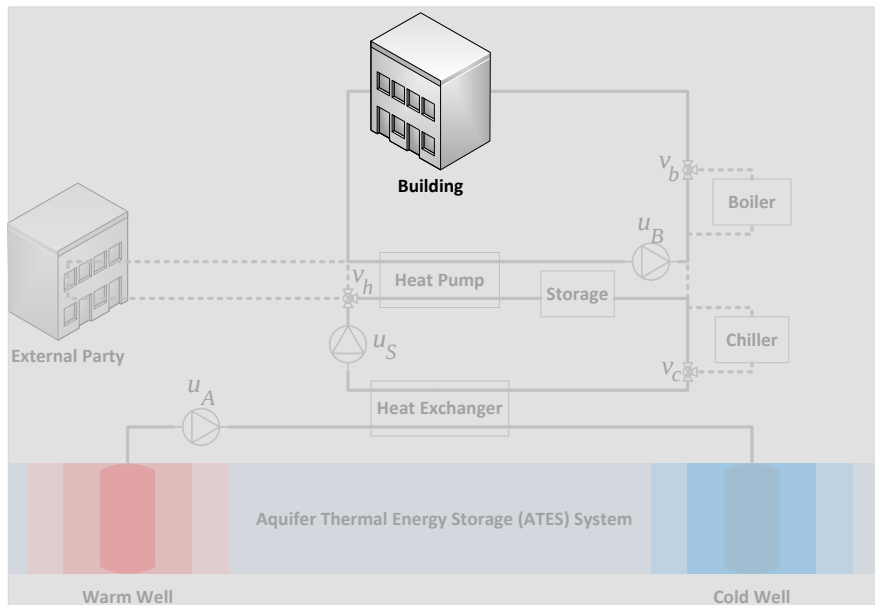
How to Develop a Predictive System Dynamics Model?



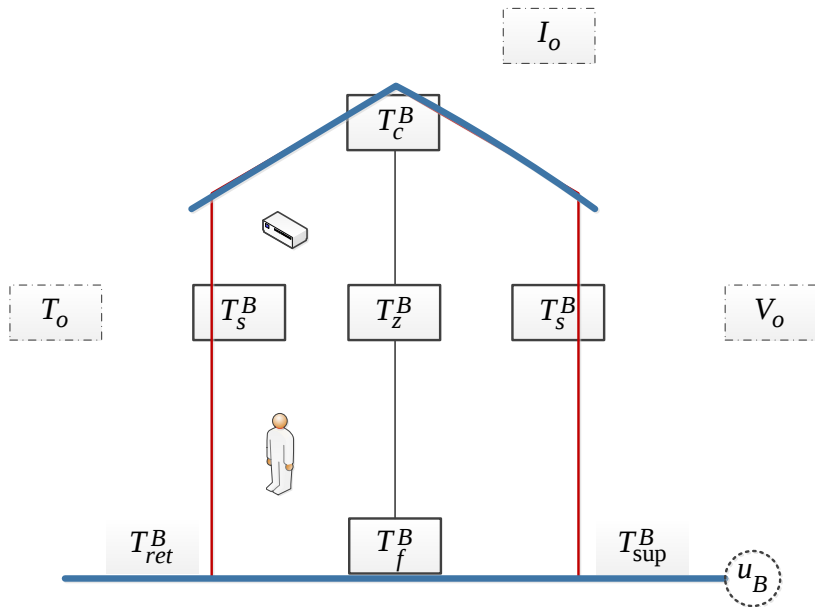
Outline

- ① Single Agent System Dynamics
- ② Control Problem Formulation
- ③ Simulation Study
- ④ Conclusions

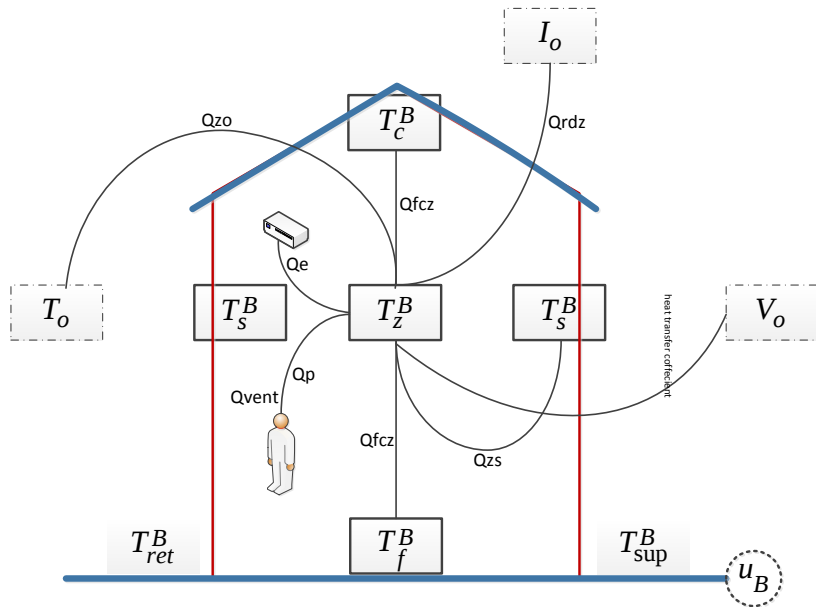
Single Agent System



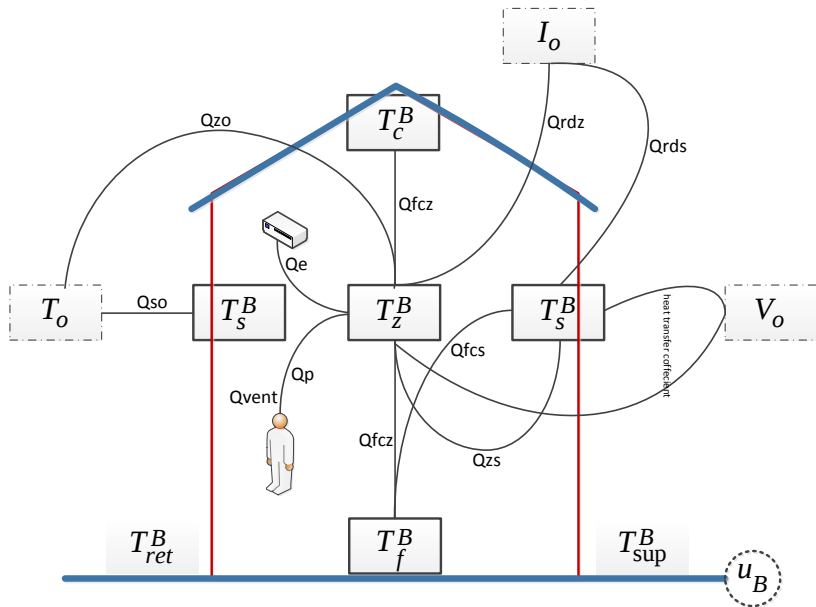
Building Thermal Comfort Relations



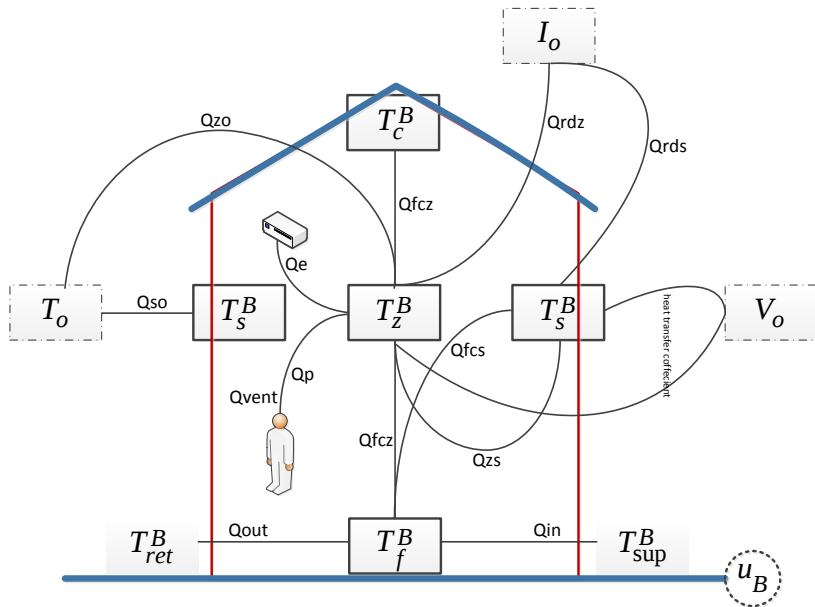
Building Thermal Comfort Relations



Building Thermal Comfort Relations



Building Thermal Comfort Relations



Building Thermal Comfort Model Formulation

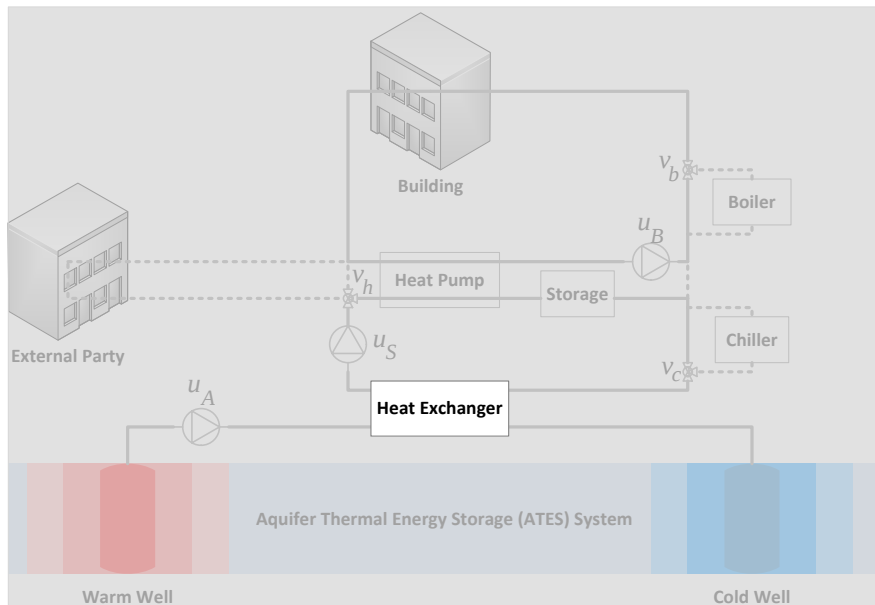
We define the following model:

Building Dynamical Model

$$\begin{aligned}\mathbf{x}_{B,k+1} &= \mathbf{x}_{B,k} + \mathbf{f}_B(\mathbf{x}_{B,k}, \mathbf{u}_{B,k}, \nu_{B,k}, \nu_{Bext,k})\tau \\ \mathbf{y}_{B,k} &= \mathbf{g}_B(\mathbf{x}_{B,k}, \mathbf{u}_{B,k})\end{aligned}$$

- Building inside variables (states): $\mathbf{x}_{B,k} \in \mathbb{R}^3$
- Building outside variables (uncertain): $\nu_{Bext,k} \in \mathbb{R}^3$
- Pump flow rate variable (control): $\mathbf{u}_{B,k}$
- Supplied water temperature: $\nu_{B,k}$
- Returned water temperature: $\mathbf{y}_{B,k}$
- Sampling period: τ

Single Agent System

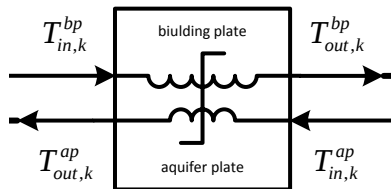


Heat Exchanger Model

A countercurrent heat exchanger is used and it presents via a static model.

Static Model Variables:

- Input water temperatures:
 $\nu_{he,k} \in \mathbb{R}^2$
- Pump flow rates
(control variables): $u_{A,k}, u_{S,k}$
- Output water temperatures:
 $y_{he,k} \in \mathbb{R}^2$

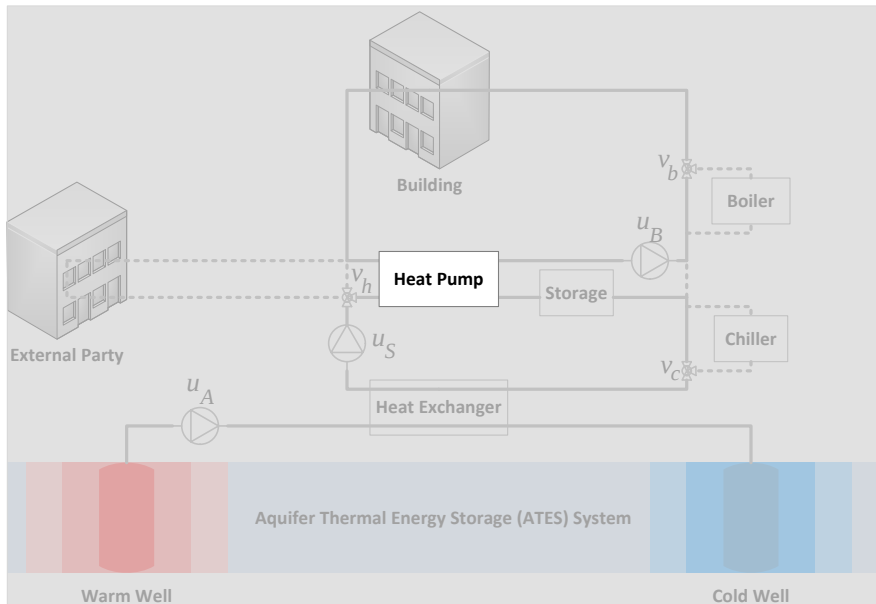


Heat Exchanger

Heat Exchanger Static Model

$$y_{he,k} = H(\nu_{he,k}, u_{A,k}, u_{S,k})$$

Single Agent System

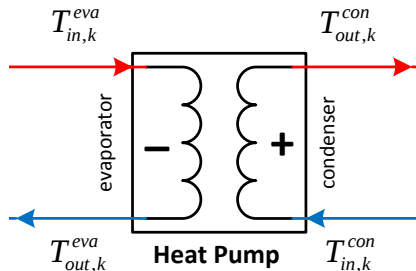


Heat Pump Model

An electrical water to water heat pump is used with static model.

Static Model Variables:

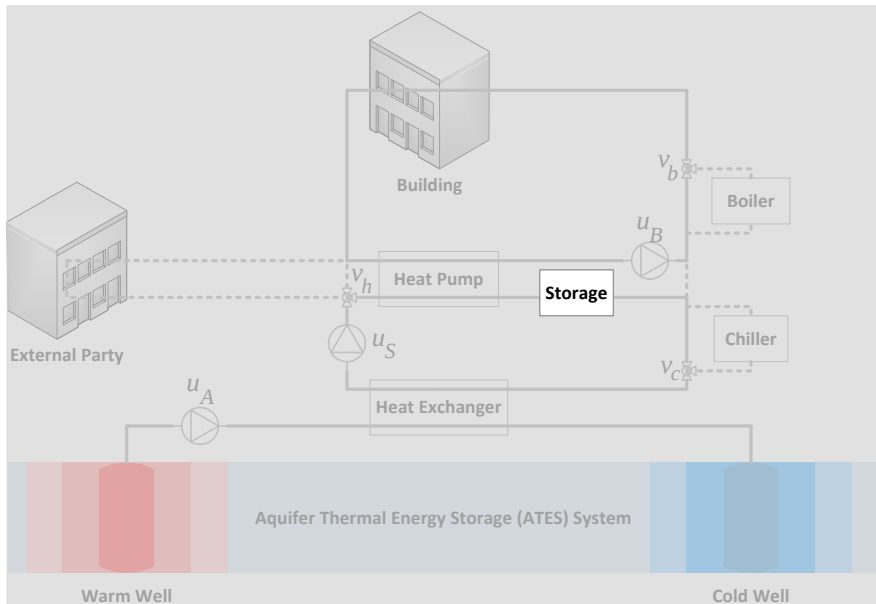
- Input water temperatures:
 $\nu_{hp,k} \in \mathbb{R}^2$
- Pump flow rates
(control variables): $u_{B,k}, u_{S,k}$
- Output water temperatures:
 $y_{hp,k} \in \mathbb{R}^2$



Heat Pump Static Model

$$y_{hp,k} = P(\nu_{hp,k}, u_{B,k}, u_{S,k})$$

Single Agent System



Storage Tank Model

We define an storage tank model with the following first order difference equations:

$$V_{s,k+1} = V_{s,k} + V_{in,k} - V_{out,k}$$

$$T_{s,k+1} = \frac{V_{s,k}}{V_{s,k} + V_{in,k}} T_{s,k} + \frac{V_{in,k}}{V_{s,k} + V_{in,k}} T_{in,k}$$

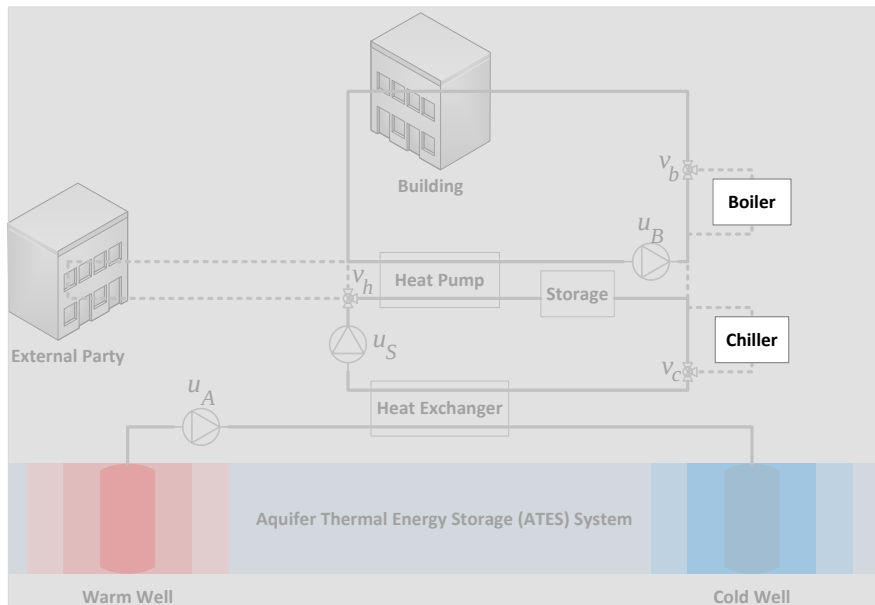
Storage Dynamical Model

$$\mathbf{x}_{S,k+1} = \mathbf{f}_S(\mathbf{x}_{S,k}, \mathbf{u}_{S,k}, \nu_{S,k})$$

$$\mathbf{y}_{S,k} = \mathbf{g}_S(\mathbf{x}_{S,k})$$

- Tank temperature and volume variables (state): $\mathbf{x}_{S,k} \in \mathbb{R}^2$
- Pump flow rate variable (control): $\mathbf{u}_{S,k}$
- Input water temperature: $\nu_{S,k}$
- Output water temperature: $\mathbf{y}_{S,k}$

Single Agent System



Boiler and Chiller Model

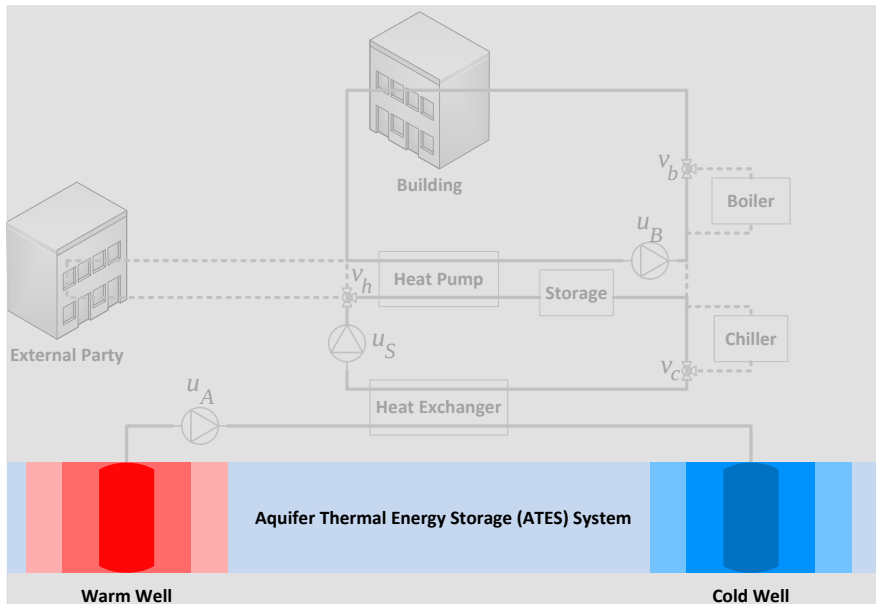
We define the boiler and chiller water temperatures with the following relations:

$$\text{Boiler: } \begin{cases} T_{out,k}^{\text{boi}} = 90^{\circ}\text{C} \\ T_{in,k}^{\text{boi}} = T_{\text{bypass},k} \\ u_{b,k} = v_{b,k} u_{B,k} \end{cases}$$

$$\text{Chiller: } \begin{cases} T_{out,k}^{\text{chi}} = 5^{\circ}\text{C} \\ T_{in,k}^{\text{chi}} = T_{\text{bypass},k} \\ u_{c,k} = v_{c,k} u_{S,k} \end{cases}$$

- Boiler valve position (control): $v_{b,k} \in [0, 1]$
- Chiller valve position (control): $v_{c,k} \in [0, 1]$

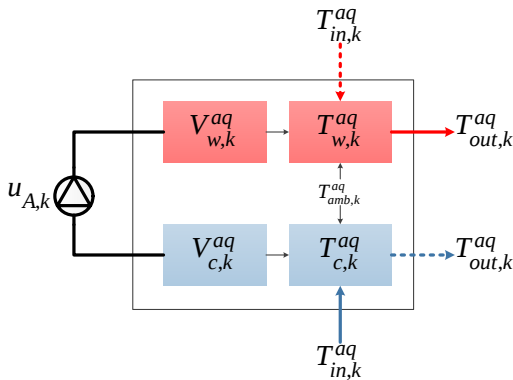
Single Agent System



Aquifer Thermal Energy Storage System Principle

Similar modeling as the storage model by introducing different modes:

- Water is taken from one of the wells and is injected into the counterpart well.
- Taken water has constant temperature until the aquifer water temperature dominates.
- Injected water has gained thermal energy and it is stored for the next upcoming season.



Aquifer Thermal Energy Storage System Model

We define the following Model:

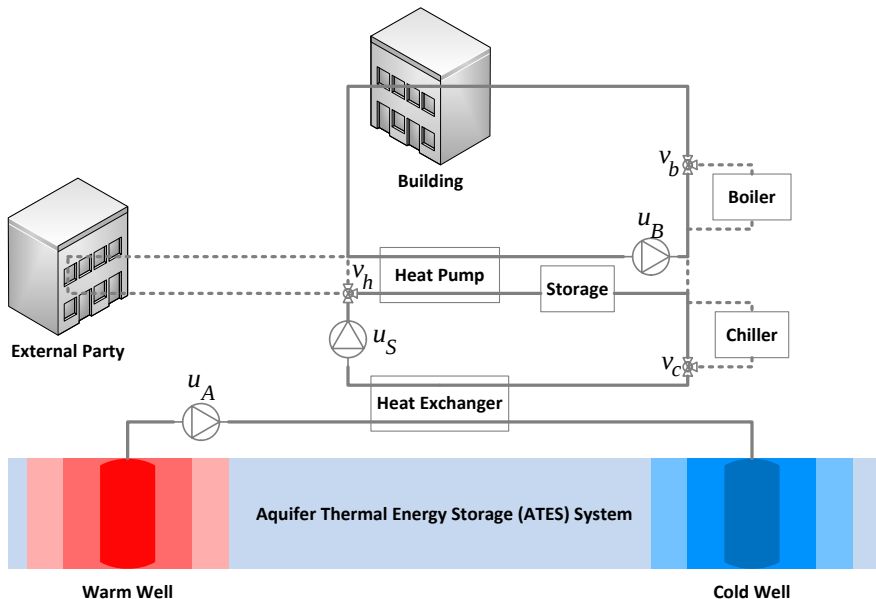
ATES system Dynamical Model

$$\mathbf{x}_{A,k+1} = \mathbf{f}_A(\mathbf{x}_{A,k}, \mathbf{u}_{A,k}, \nu_{A,k}, \mathbf{s}_{w,k}, \mathbf{s}_{c,k})$$

$$\mathbf{y}_{A,k} = \mathbf{g}_A(\mathbf{x}_{A,k}, \mathbf{s}_{w,k}, \mathbf{s}_{c,k})$$

- Wells temperature and volume variables (state): $\mathbf{x}_{A,k} \in \mathbb{R}^4$
- Pump flow rate variable (control): $\mathbf{u}_{A,k}$
- Output water temperature: $\mathbf{y}_{A,k}$
- Input water temperature: $\nu_{A,k}$

Interconnections Between Each Subsystem



Interconnections Between Each Subsystem

① **ATES system:** $\nu_{A,k} := T_{in,k}^{aq}, \quad y_{A,k} := T_{out,k}^{aq}$

- $T_{in,k}^{aq} = T_{out,k}^{ap}$

② **Heat exchanger:** $\nu_{he,k} := [T_{in,k}^{ap}, T_{in,k}^{bp}], \quad y_{he,k} := [T_{out,k}^{ap}, T_{out,k}^{bp}]$

- $T_{in,k}^{ap} = T_{out,k}^{aq}$ and $T_{in,k}^{bp} = (1 - \nu_{c,k})T_{s,k} + \nu_{c,k}T_{out,k}^{chi}$

③ **Heat pump:** $\nu_{hp,k} := [T_{in,k}^{con}, T_{in,k}^{eva}], \quad y_{hp,k} := [T_{out,k}^{con}, T_{out,k}^{eva}]$

- $T_{in,k}^{con} = s_{n,k}(s_{w,k}T_{out,k}^{bp} + s_{c,k}T_{ret,k}^B) + (1 - s_{n,k})(s_{w,k}T_{out,k}^{ext} + s_{c,k}T_{ret,k}^B)$

- $T_{in,k}^{eva} = s_{n,k}(s_{c,k}T_{out,k}^{bp} + s_{w,k}T_{ret,k}^B) + (1 - s_{n,k})(s_{w,k}T_{out,k}^{ext} + s_{c,k}T_{ret,k}^B)$

④ **Storage model:** $\nu_{S,k} := T_{in,k}, \quad y_{S,k} := T_{out,k}^s$

- $T_{in,k}^s = \nu_{h,k}(s_{w,k}T_{out,k}^{con} + s_{c,k}T_{out,k}^{eva}) + (1 - \nu_{h,k})T_{ret,k}^B$

⑤ **Building model:** $\nu_{B,k} := T_{sup,k}^B, \quad y_{B,k} := T_{ret,k}^B$

$$T_{sup,k}^B = \nu_{h,k}(s_{w,k}T_{out,k}^{eva} + s_{c,k}((1 - \nu_{b,k})T_{out,k}^{con} + \nu_{b,k}T_{out,k}^{boi})) + (1 - \nu_{h,k})T_{out,k}^{bp}$$

Single Agent Representation

Consider compact formulation of dynamical agent system:

Single Agent Model

$$\mathbf{x}_{k+1} = \mathbf{f}(\mathbf{x}_k, \mathbf{u}_k, \mathbf{v}_k, \mathbf{s}_k, \mathbf{w}_k)$$

- State variables: $\mathbf{x}_k := [\mathbf{x}_{B,k}, \mathbf{x}_{S,k}, \mathbf{x}_{A,k}] \in \mathbb{R}^9$
- Pump flow rate variables: $\mathbf{u}_k := [\mathbf{u}_{B,k}, \mathbf{u}_{S,k}, \mathbf{u}_{A,k}] \in \mathbb{R}^3$
- Valve position variables: $\mathbf{v}_k := [\mathbf{v}_{b,k}, \mathbf{v}_{c,k}, \mathbf{v}_{h,k}] \in [0, 1]^3$
- Operating mode variables: $\mathbf{s}_k := [\mathbf{s}_{w,k}, \mathbf{s}_{c,k}, \mathbf{s}_{n,k}] \in \{0, 1\}^3$
- Uncertain variables: $\mathbf{w}_k := [\mathbf{T}_{o,k}, \mathbf{l}_{o,k}, \mathbf{V}_{o,k}] \subseteq \Delta \in \mathbb{R}^3$
- State variables are available at each sampling time k .

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Control Problem Formulation

We formulate an optimization problem as follows:

$$\begin{array}{ll} \min_{\{u_k, v_k\}_{k=1}^N} & \text{Objective Function: Reference Tracking} \\ \text{subject to:} & \begin{array}{l} \text{Nonlinear System Dynamics} \\ \text{State and Control Bounds} \\ \text{Valves, Modes and Uncertainty Sets} \\ \text{Heat Exchanger Capacity Constraints} \\ \text{Heat Pump Capacity Constraints} \end{array} \end{array}$$

Proposed Formulation

Stochastic Mixed-Integer Nonlinear Optimization Problem

Control Problem Formulation

We formulate an optimization problem as follows:

$$\begin{aligned} & \min_{\{u_k, v_k\}_{k=1}^N} && \mathbb{E} \left[\sum_{k=1}^N \gamma (T_{z,k}^B - T_{\text{set}})^2 \right] \\ & \text{subject to:} && \begin{aligned} & \text{Nonlinear System Dynamics} \\ & \text{State and Control Bounds} \\ & \text{Valves, Modes and Uncertainty Sets} \\ & \text{Heat Exchanger Capacity Constraints} \\ & \text{Heat Pump Capacity Constraints} \end{aligned} \end{aligned}$$

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State and Control Bounds

Valves, Modes and Uncertainty Sets

Heat Exchanger Capacity Constraints

Heat Pump Capacity Constraints

Proposed Formulation

Stochastic Mixed-Integer Nonlinear Optimization Problem

Control Problem Formulation

We formulate an optimization problem as follows:

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Control Problem Formulation

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Heat Exchanger Capacity Constraints

Heat Pump Capacity Constraints

Proposed Formulation

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Control Problem Formulation

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Heat Pump Capacity Constraints

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Control Problem Formulation

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Proposed Formulation

Stochastic Mixed-Integer Nonlinear Optimization Problem

Control Problem Formulation

We formulate an optimization problem as follows:

$$\begin{aligned} \min_{\{u_k, v_k\}_{k=1}^N} \quad & \mathbb{E} \left[\sum_{k=1}^N \gamma (T_{z,k}^B - T_{\text{set}})^2 \right] \\ \text{subject to:} \quad & \mathbf{x}_{k+1} = \mathbf{f}(\mathbf{x}_k, \mathbf{u}_k, \mathbf{v}_k, \mathbf{s}_k, \mathbf{w}_k) \\ & \mathbf{x}_{\min} \leq \mathbf{x}_k \leq \mathbf{x}_{\max}, \quad \mathbf{u}_{\min} \leq \mathbf{u}_k \leq \mathbf{u}_{\max} \\ & 0 \leq \mathbf{v}_k \leq 1, \quad \mathbf{s}_k \in \{0, 1\}, \quad \mathbf{w}_k \in \Delta \\ & \nu_{\text{he}}^{\min} \leq \nu_{\text{he},k} \leq \nu_{\text{he}}^{\max}, \quad y_{\text{he}}^{\min} \leq y_{\text{he},k} \leq y_{\text{he}}^{\max} \\ & \nu_{\text{hp}}^{\min} \leq \nu_{\text{hp},k} \leq \nu_{\text{hp}}^{\max}, \quad y_{\text{hp}}^{\min} \leq y_{\text{hp},k} \leq y_{\text{hp}}^{\max} \end{aligned}$$

Proposed Formulation

Stochastic Mixed-Integer Nonlinear Optimization Problem

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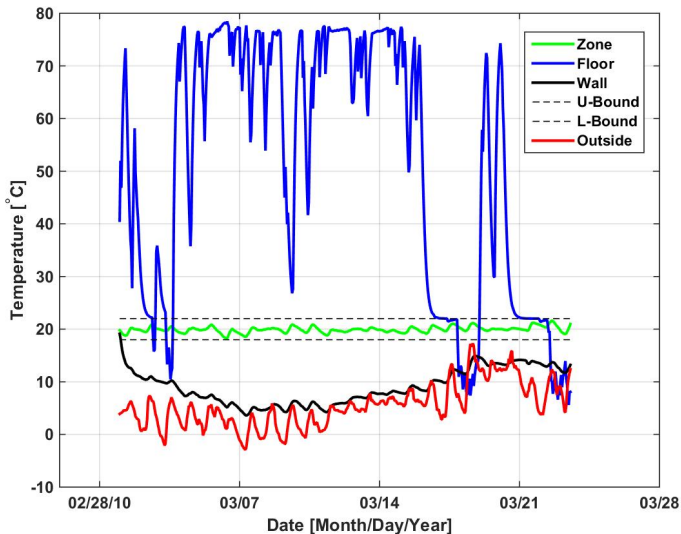
Simulation Study

A single agent model control problem formulation:

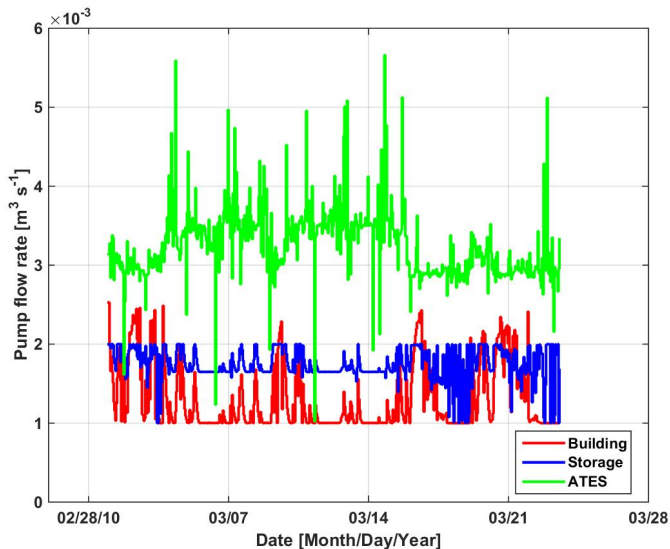
- Sampling period: **1h**
- Prediction horizon: **24h**
- No integer variables (fixed)
- No stochastic terms (deterministic controller)
- Linear approximation of HP & HE complex subsystems
- Remove complex constraints of HP & HE:

$$\nu_{\text{he}}^{\min} \leq \nu_{\text{he},k} \leq \nu_{\text{he}}^{\max}, \quad y_{\text{he}}^{\min} \leq y_{\text{he},k} \leq y_{\text{he}}^{\max}$$
$$\nu_{\text{hp}}^{\min} \leq \nu_{\text{hp},k} \leq \nu_{\text{hp}}^{\max}, \quad y_{\text{hp}}^{\min} \leq y_{\text{hp},k} \leq y_{\text{hp}}^{\max}$$

Simulation Results



Simulation Results



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Concluding Remarks

- ATES System Dynamics Model
- Building Climate Comfort System Dynamics Model
- Integrated ATES System into Building Climate Comfort System
- Important Features:
 - Complete mathematical models of building thermal equipment
 - Developed model is highly complex and nonlinear; it can be considered as a thermal energy demand of a building

- Complete Predictive Model of the ATES System
[Rostampour et al., EGU, 2017]
- ATES in Smart Thermal Grids + Preventing Mutual Interactions
[Rostampour et al., IFAC, 2017]
- Distributed Stochastic MPC for ATES in Smart Thermal Grids
[Rostampour et al., Submitted, 2017]

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